

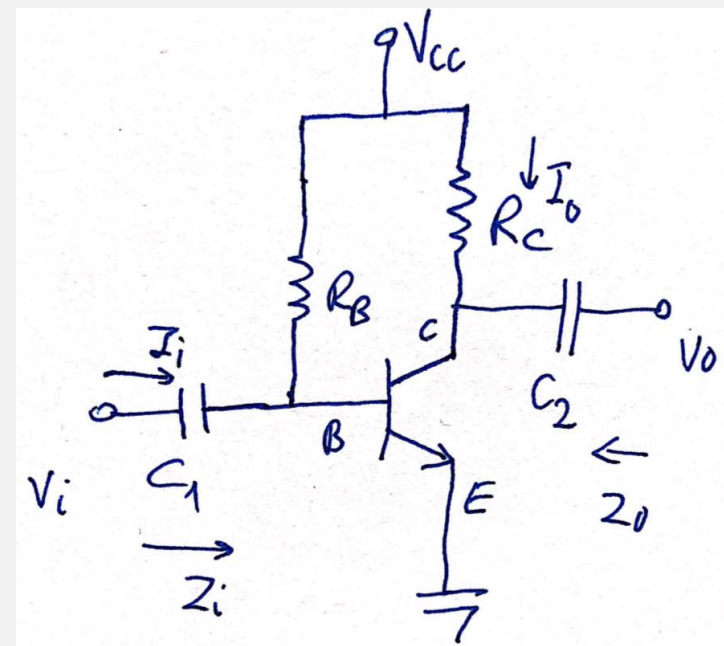


BME 202 Electronics

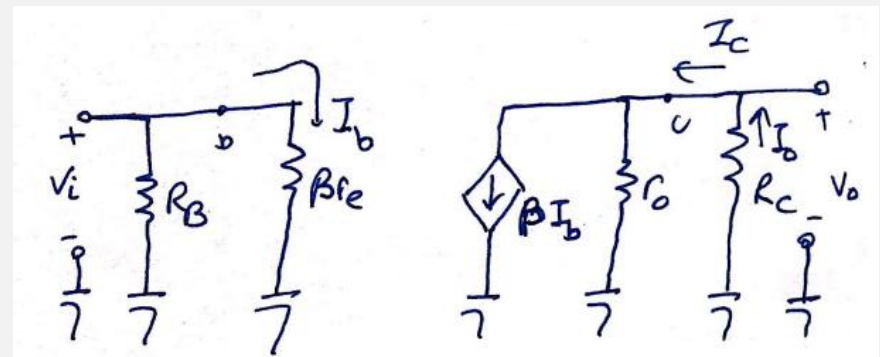
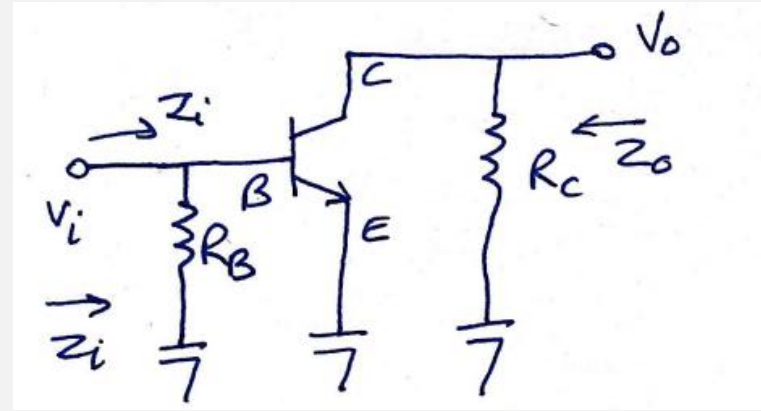
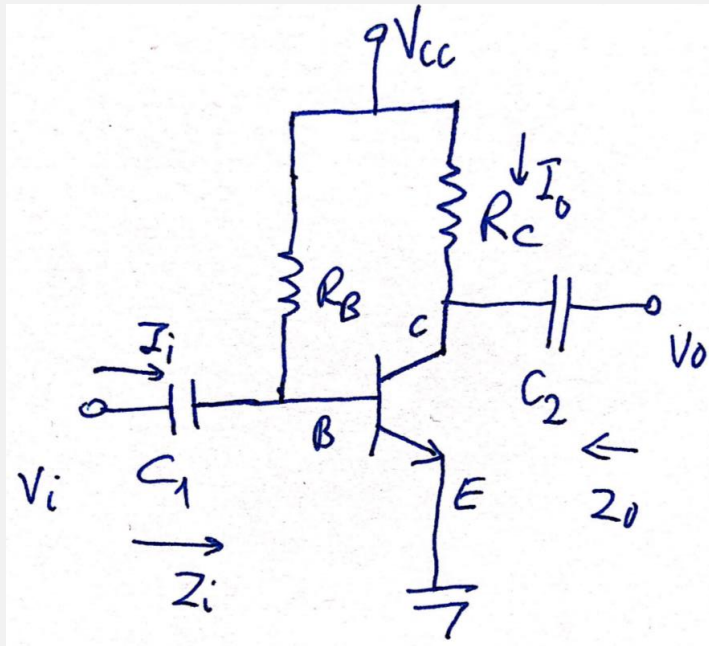
Lecture 8: BJT – AC Analysis Part 2

Common-Emitter Fixed-Bias Configuration

- The input is applied to the base
- The output is taken from the collector
- High input impedance
- Low output impedance
- High voltage and current gain
- Phase shift between input and output is 180°

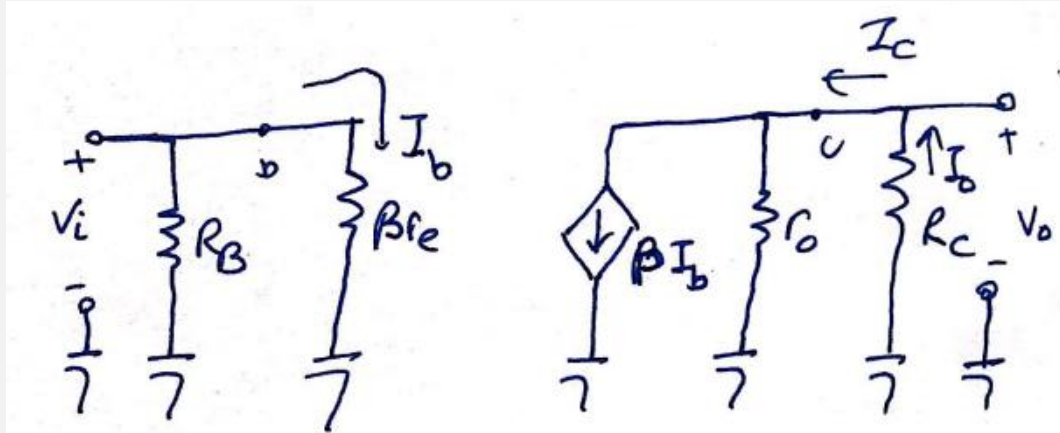


Common-Emitter Fixed-Bias Configuration



r_e model

Common-Emitter Fixed-Bias Calculations



Input impedance:

$$Z_i = R_B // \beta r_e$$

$$Z_i \cong \beta r_e \quad | \quad R_E \geq 10\beta r_e$$

Output impedance:

$$Z_o = R_C // r_o$$

$$Z_o \cong R_C \quad | \quad r_o \geq 10R_C$$

Voltage gain:

$$A_v = \frac{V_o}{V_i} = -\frac{(R_C // r_o)}{r_e}$$

$$A_v = -\frac{R_C}{r_e} \quad | \quad r_o \geq 10R_C$$

Current gain:

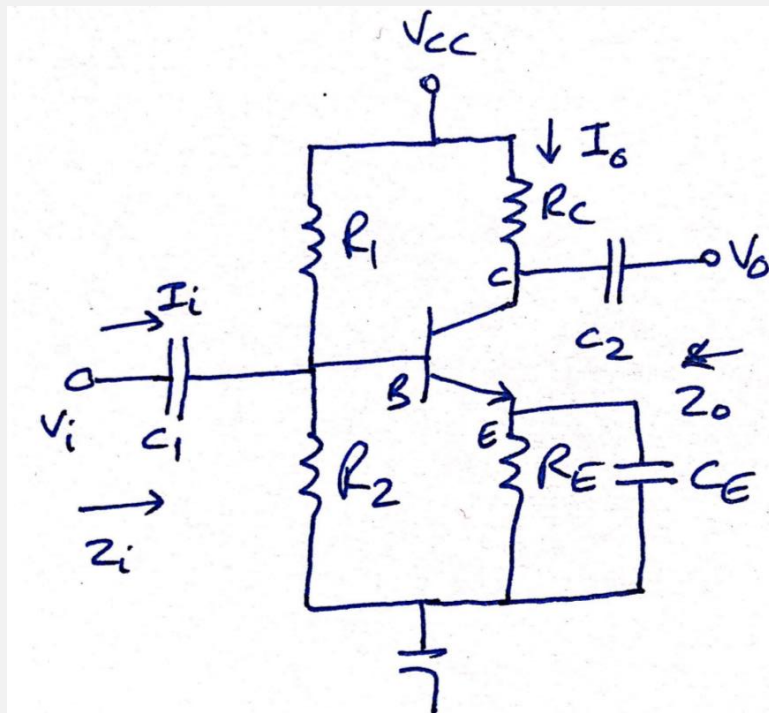
$$A_i = \frac{I_o}{I_i} = \frac{\beta R_B r_o}{(r_o + R_C)(R_B + \beta r_e)}$$

$$A_i \cong \beta \quad | \quad r_o \geq 10R_C, R_B \geq 10\beta r_e$$

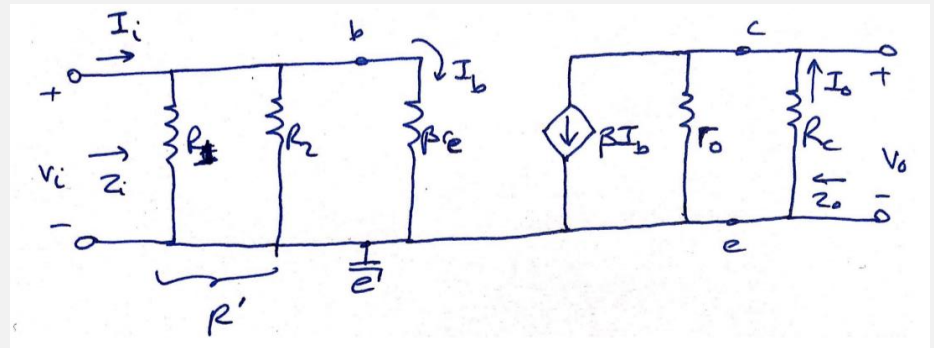
Current gain from voltage gain:

$$A_i = -A_v \frac{Z_i}{R_C}$$

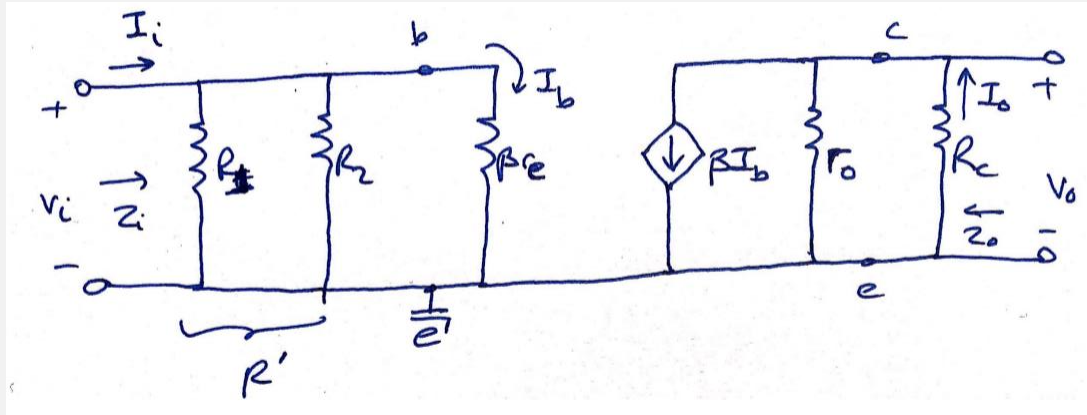
Common-Emitter Voltage-Divider Bias



r_e model requires you to determine β , r_e , and r_o .



Common-Emitter Voltage-Divider Bias Calculations



Input impedance

$$R' = R_1 \parallel R_2$$

$$Z_i = R' \parallel \beta r_e$$

Output impedance

$$Z_o = R_C \parallel r_o$$

$$Z_o \cong R_C \Big|_{r_o \geq 10R_C}$$

Current gain

$$A_i = \frac{I_o}{I_i} = \frac{\beta R' r_o}{(r_o + R_C)(R' + \beta r_e)}$$

$$A_i = \frac{I_o}{I_i} \cong \frac{\beta R'}{R' + \beta r_e} \Big|_{r_o \geq 10R_C}$$

$$A_i = \frac{I_o}{I_i} \cong \beta \Big|_{r_o \geq 10R_C, R' \geq 10\beta r_e}$$

Voltage gain

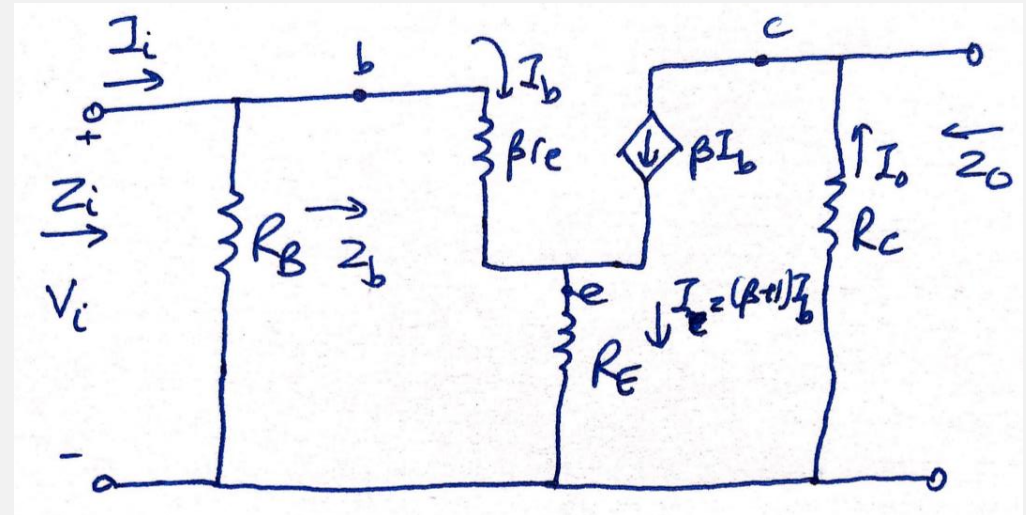
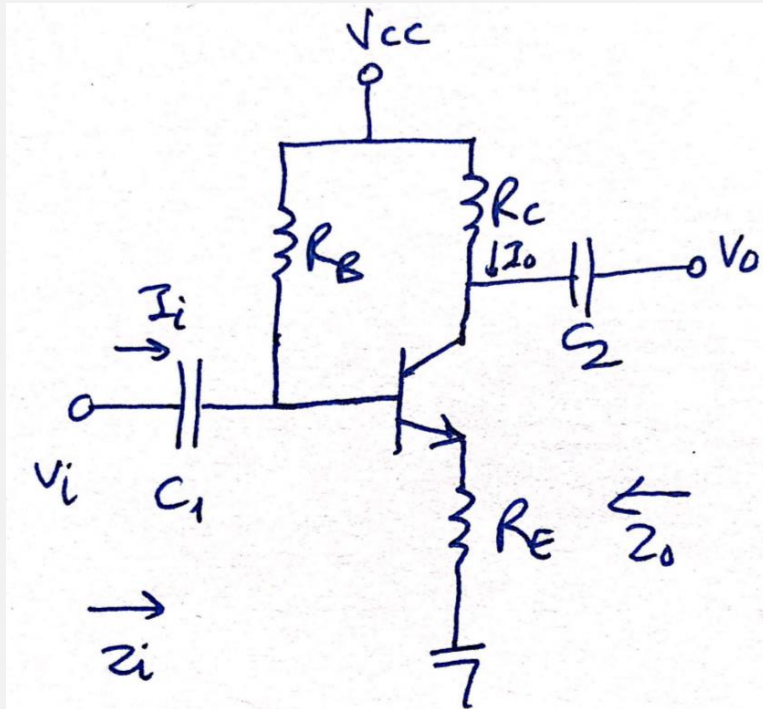
$$A_v = \frac{V_o}{V_i} = \frac{-R_C \parallel r_o}{r_e}$$

$$A_v = \frac{V_o}{V_i} \cong -\frac{R_C}{r_e} \Big|_{r_o \geq 10R_C}$$

Current gain from A_v

$$A_i = -A_v \frac{Z_i}{R_C}$$

Common-Emitter Emitter-Bias Configuration



Impedance Calculations

Input impedance:

$$Z_i = R_B // Z_b$$

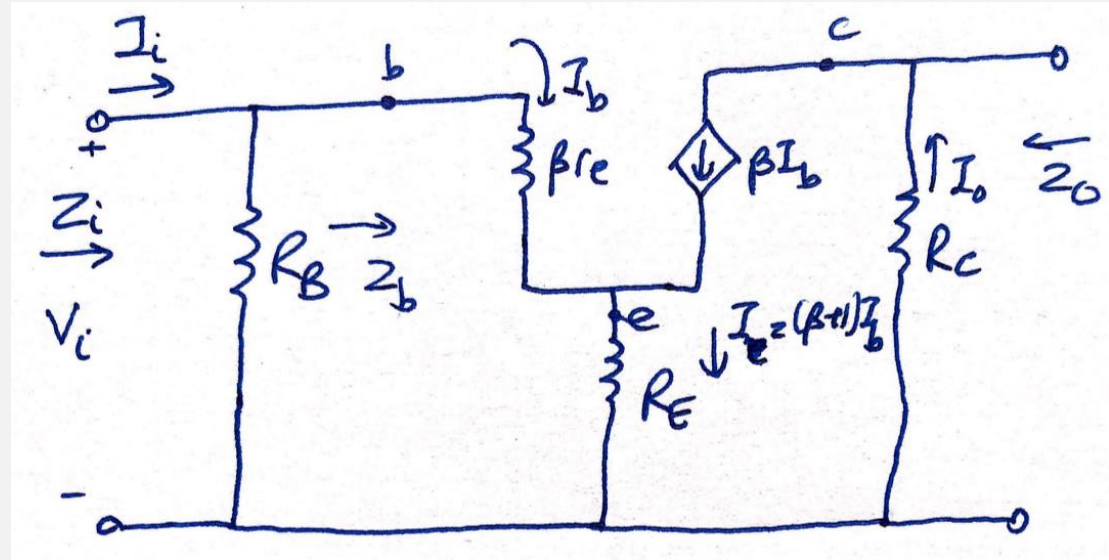
$$Z_b = \beta r_e + (\beta + 1)R_E$$

$$Z_b \cong \beta(r_e + R_E)$$

$$Z_b \cong \beta R_E$$

Output impedance:

$$Z_o = R_C$$



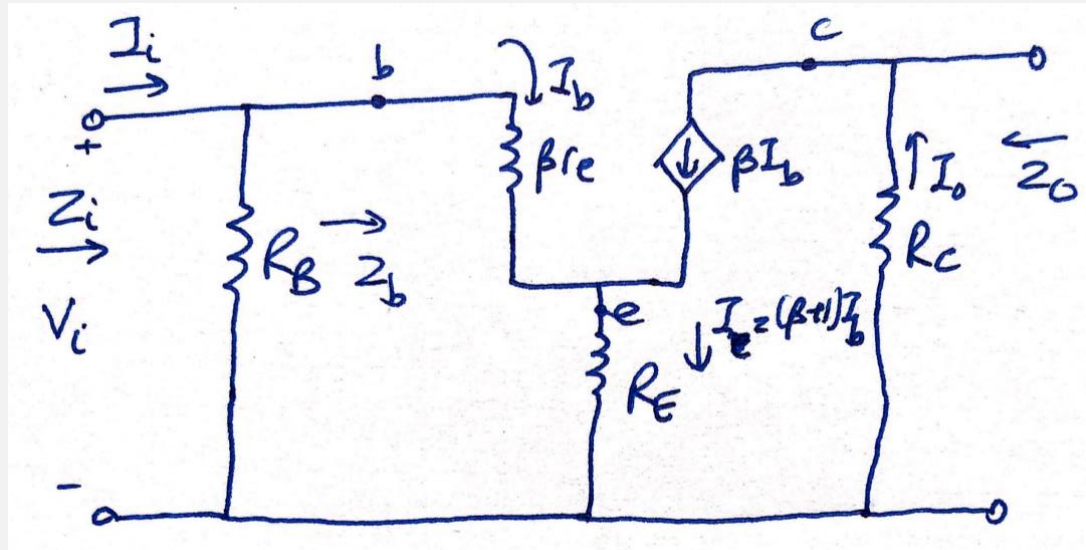
Gain Calculations

Voltage gain:

$$A_v = \frac{V_o}{V_i} = -\frac{\beta R_C}{Z_b}$$

$$A_v = \frac{V_o}{V_i} = -\frac{R_C}{r_e + R_E} \Big|_{Z_b = \beta(r_e + R_E)}$$

$$A_v = \frac{V_o}{V_i} \cong -\frac{R_C}{R_E} \Big|_{Z_b \cong \beta R_E}$$



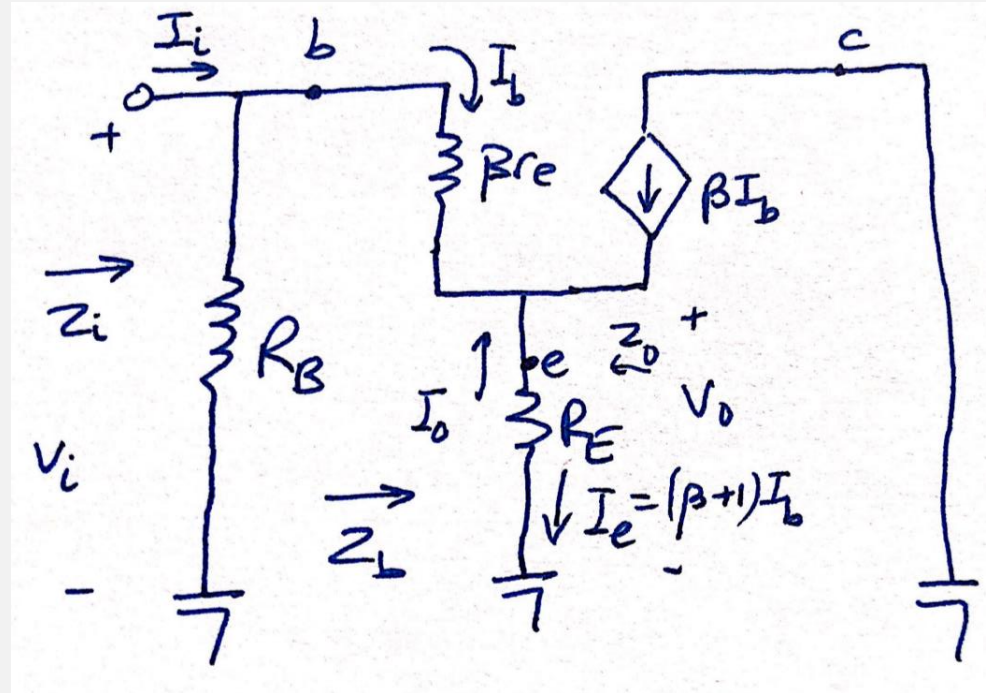
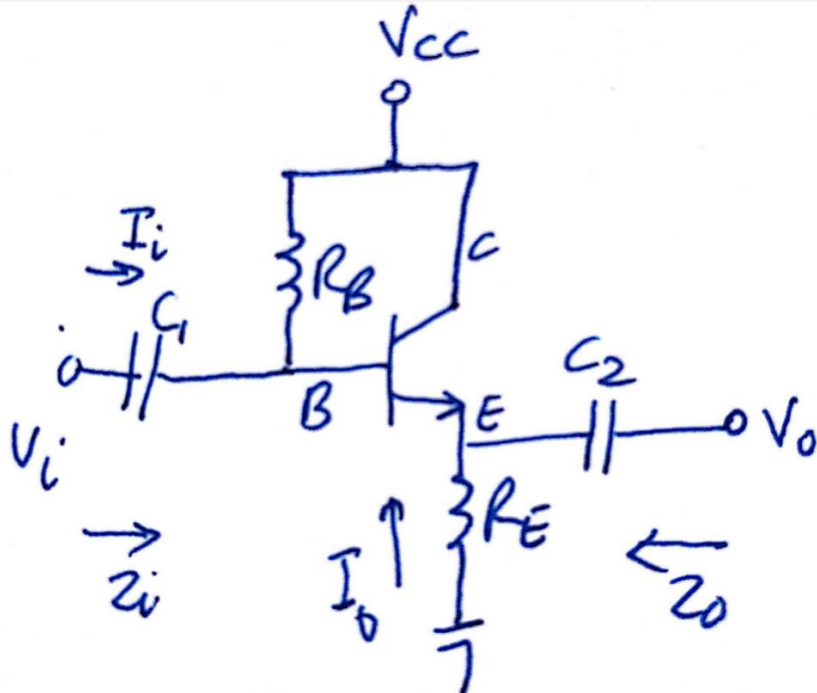
Current gain:

$$A_i = \frac{I_o}{I_i} = \frac{\beta R_B}{R_B + Z_b}$$

Current gain from A_v :

$$A_i = -A_v \frac{Z_i}{R_C}$$

Emitter-Follower Configuration



This is also known as the *common-collector* configuration.

The **input** is applied to the **base** and the **output** is taken from the **emitter**.

There is **no phase shift** between input and output.

Impedance Calculations

Input impedance:

$$Z_i = R_B // Z_b$$

$$Z_b = \beta r_e + (\beta + 1)R_E$$

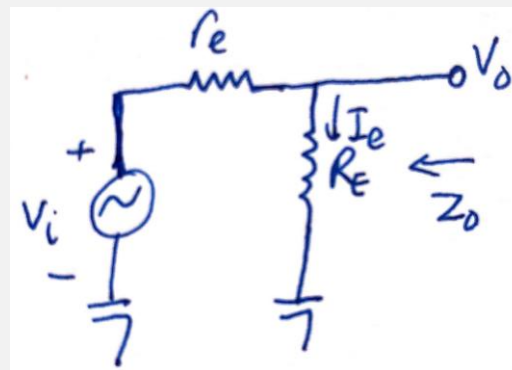
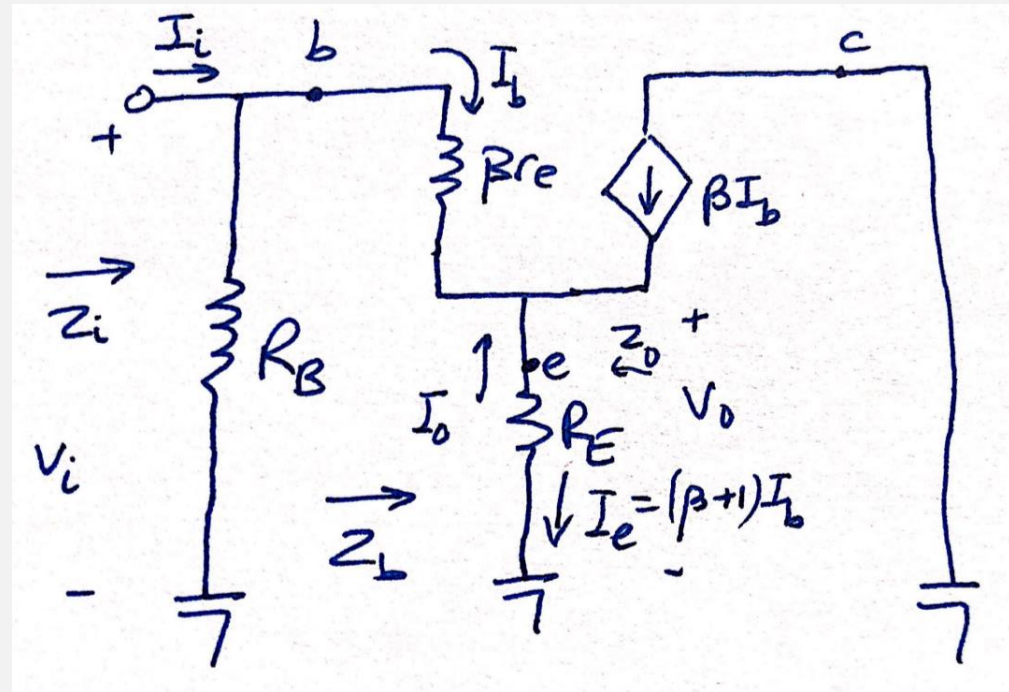
$$Z_b \cong \beta(r_e + R_E)$$

$$Z_b \cong \beta R_E$$

Output impedance:

$$Z_o = R_E // r_e$$

$$Z_o \cong r_e \Big|_{R_E \gg r_e}$$



Gain Calculations

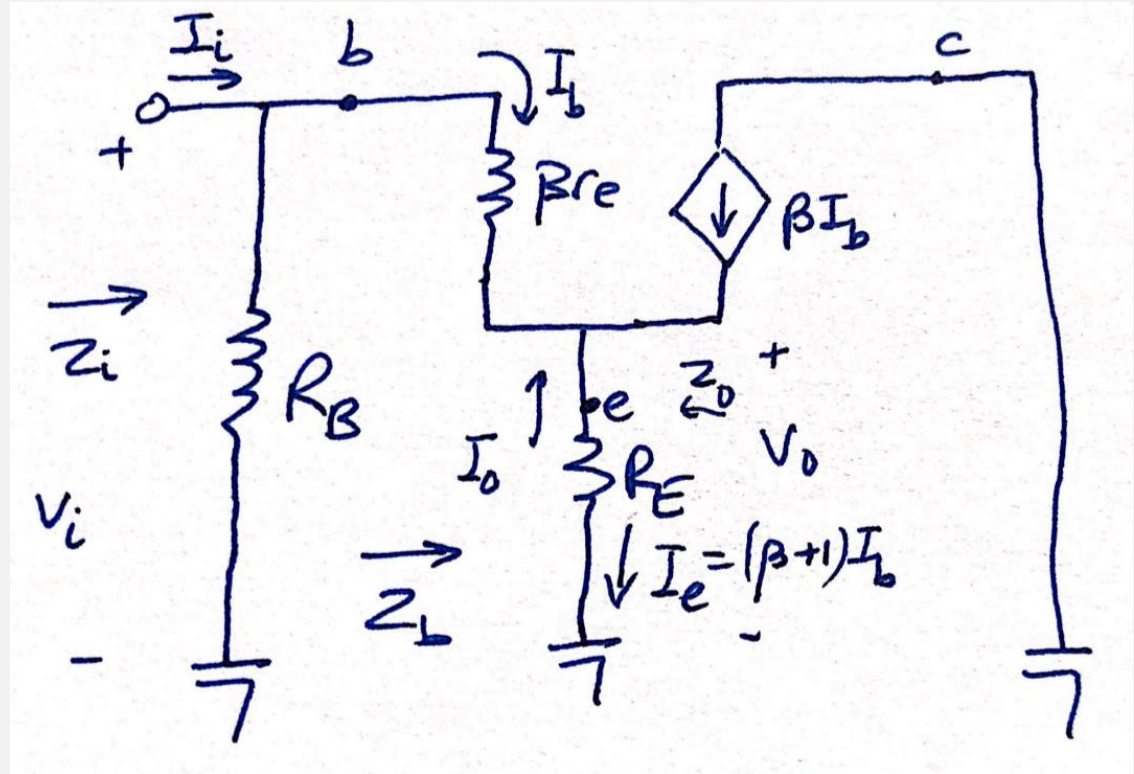
Voltage gain:

$$A_v = \frac{V_o}{V_i} = \frac{R_E}{R_E + r_e}$$

$$A_v = \frac{V_o}{V_i} \cong 1 \Big|_{R_E \gg r_e, R_E + r_e \cong R_E}$$

Current gain:

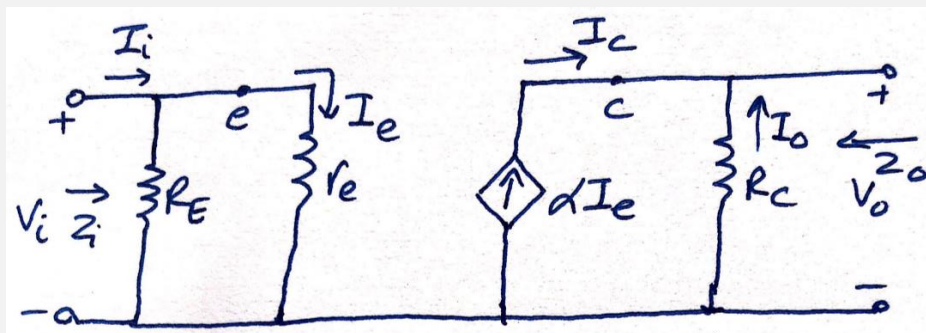
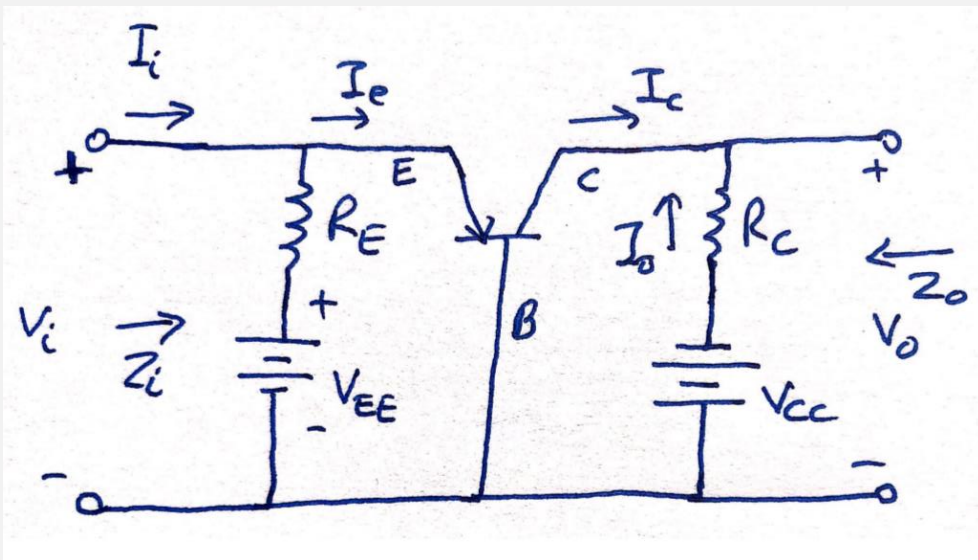
$$A_i \cong -\frac{\beta R_B}{R_B + Z_b}$$



Current gain from voltage gain:

$$A_i = -A_v \frac{Z_i}{R_E}$$

Common-Base Configuration



- The input is applied to the emitter
- The output is taken from the collector
- Low input impedance. High output impedance
- Current gain less than unity
- Very high voltage gain
- No phase shift between input and output

Calculations

Input impedance:

$$Z_i = R_E \parallel r_e$$

Output impedance:

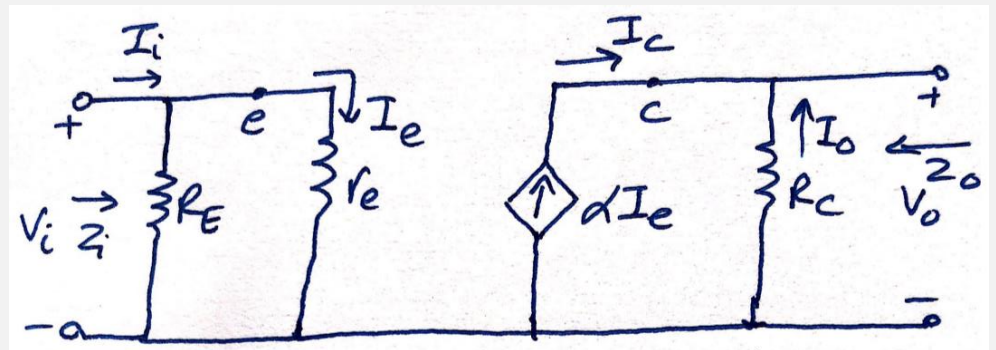
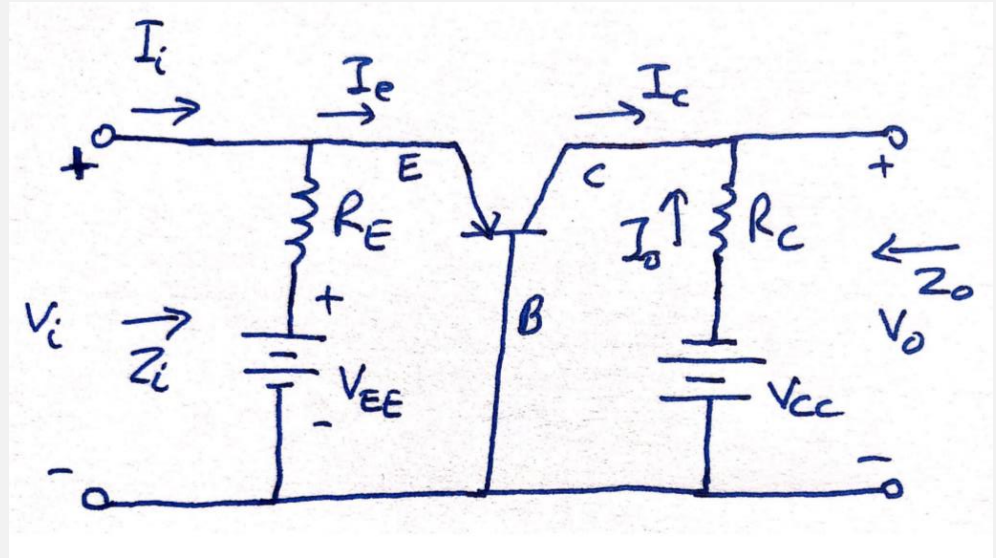
$$Z_o = R_C$$

Voltage gain:

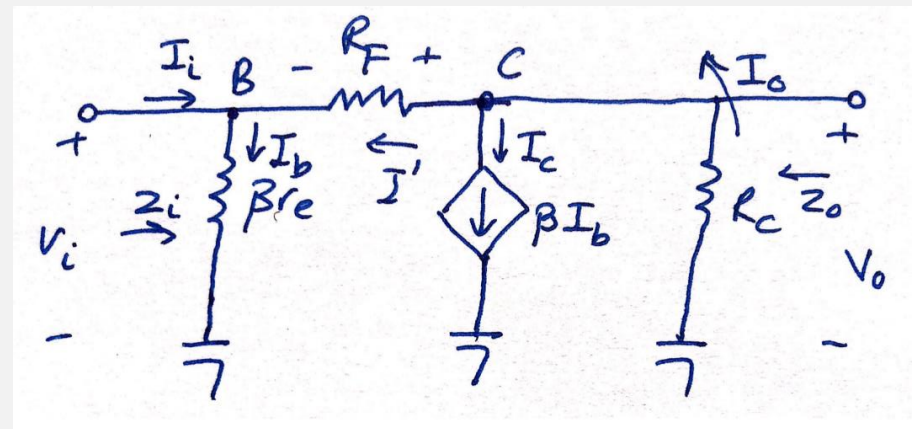
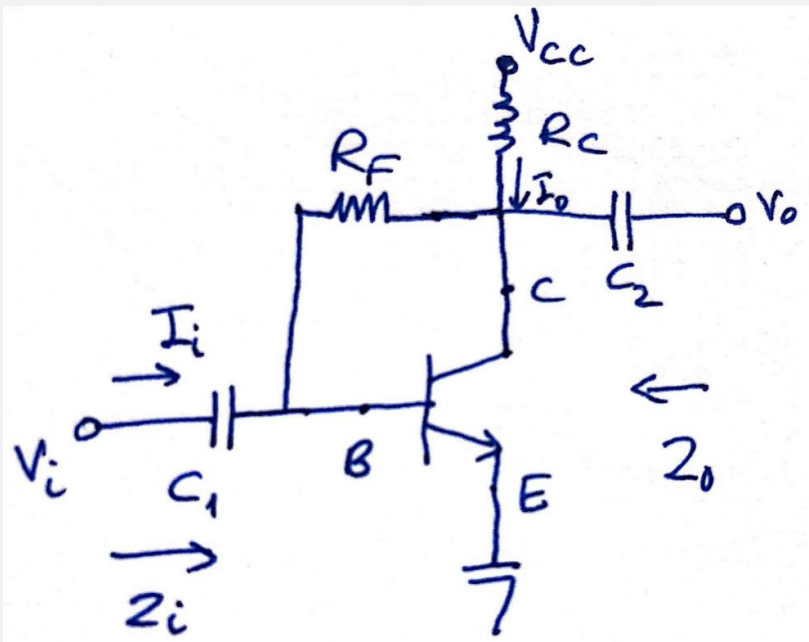
$$A_v = \frac{V_o}{V_i} = \frac{\alpha R_C}{r_e} \approx \frac{R_C}{r_e}$$

Current gain:

$$A_i = \frac{I_o}{I_i} = -\alpha \approx -1$$



Common-Emitter Collector Feedback Configuration



- A variation of the common-emitter fixed-bias configuration
- Input is applied to the base
- Output is taken from the collector
- There is a 180° phase shift between the input and output

Calculations

Input impedance: $Z_i = \frac{r_e}{\frac{1}{\beta} + \frac{R_C}{R_F}}$

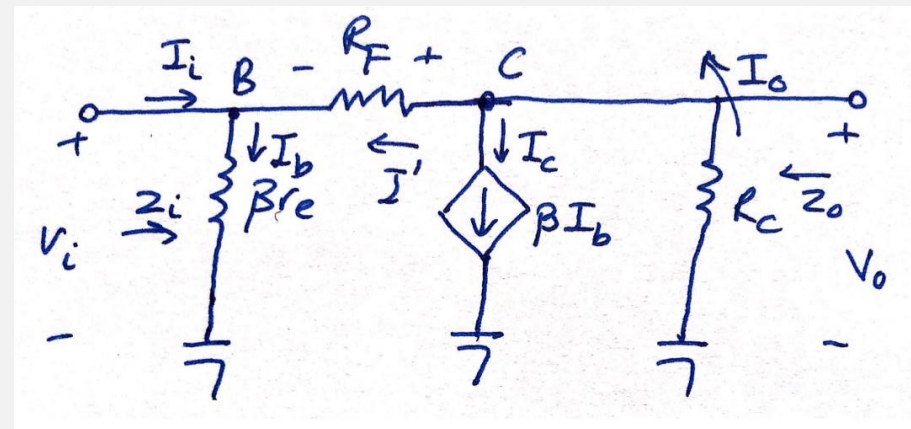
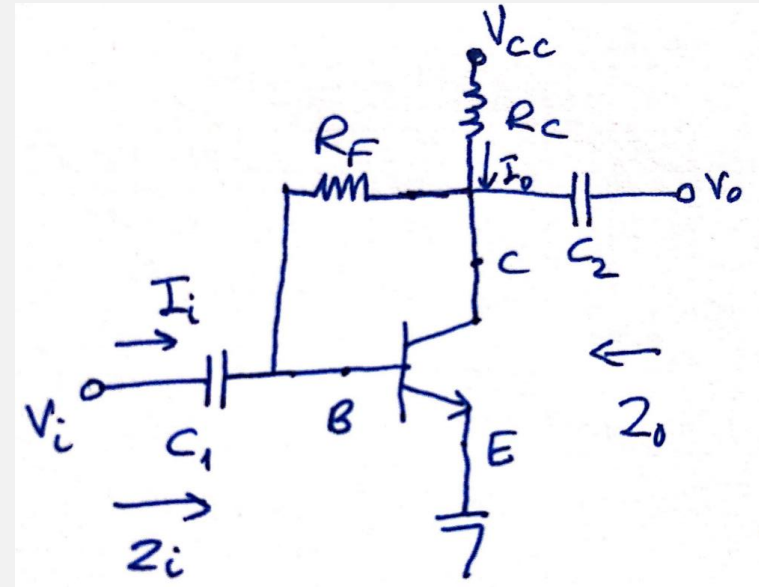
Output impedance: $Z_o \cong R_C \parallel R_F$

Voltage gain: $A_v = \frac{V_o}{V_i} = -\frac{R_C}{r_e}$

Current gain:

$$A_i = \frac{I_o}{I_i} = \frac{\beta R_F}{R_F + \beta R_C}$$

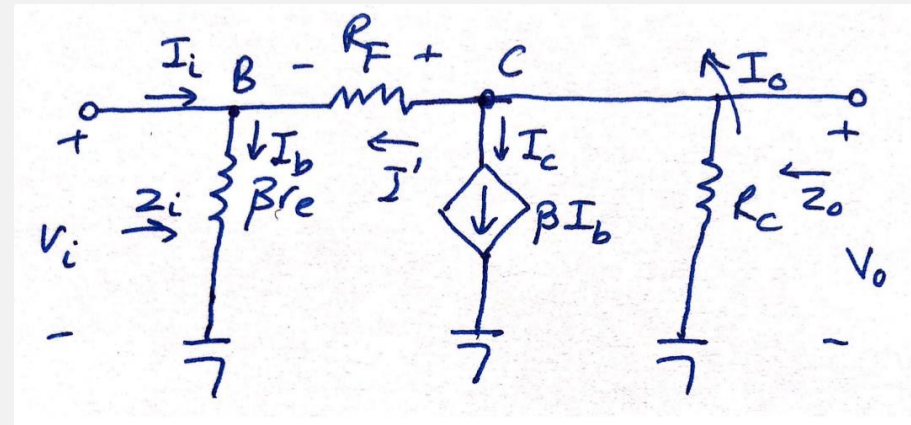
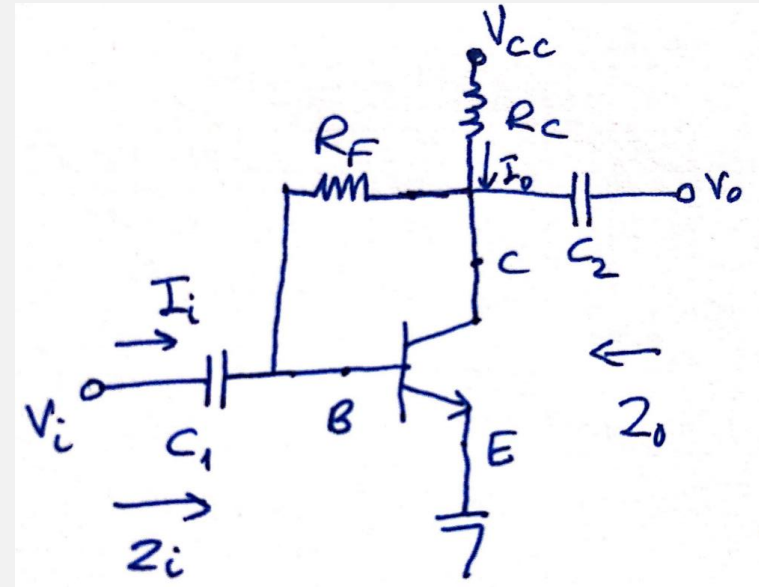
$$A_i = \frac{I_o}{I_i} \cong \frac{R_F}{R_C}$$



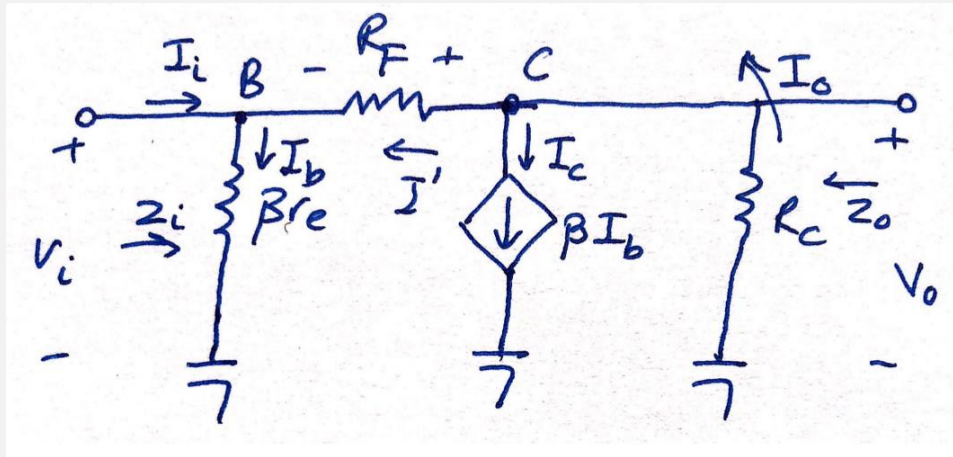
Collector DC Feedback Configuration

This is a variation of the common-emitter, fixed-bias configuration

- The input is applied to the base
- The output is taken from the collector
- There is a 180° phase shift between input and output



Calculations



Input impedance:

$$Z_i = \frac{r_e}{\frac{1}{\beta} + \frac{R_C}{R_F}}$$

Output impedance:

$$Z_o \cong R_C \parallel R_F$$

Voltage gain:

$$A_i = \frac{I_o}{I_i} = \frac{\beta R_F}{R_F + \beta R_C}$$

$$A_i = \frac{I_o}{I_i} \cong \frac{R_F}{R_C}$$

Current gain:

$$A_v = \frac{V_o}{V_i} = -\frac{R_C}{r_e}$$