# CONTROL SYSTEMS



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#### Handling the special cases - An Example A row is entirely zero

$$s^5 + 2s^4 + 24s^3 + 48s^2 - 25s - 50 = 0$$



#### Handling the special cases - An Example A row is entirely zero

$$s^{5} + 2s^{4} + 24s^{3} + 48s^{2} - 25s - 50 = 0$$

$$s^{5} \qquad 1 \qquad 24 \qquad -25$$

$$s^{4} \qquad 2 \qquad 48 \qquad -50$$

$$s^{3} \qquad 8 \qquad 96$$

$$s^{2} \qquad 24 \qquad -50$$

$$s^{1} \qquad 112.6666 \qquad 0$$

$$s^{0} \qquad -50$$
One sign change: Or of the roots is in the right half s-plane

e

#### **Final Remarks on Routh Criterion**

The goal of using Routh stability criterion is to explain whether the characteristic equation has roots on the right half s-plane.

A parameter (e.g. a gain) may change the locations of the CL poles, and Routh criterion lets us know for which range the CL system is stable.

#### **P-3 State Space Representation and Stability**



Consider the mass-springdamper system. Laws of physics lead us to

$$m\ddot{y} + b\dot{y} + ky = u$$

Let us define the state as

 $x_1(t) = y(t)$  $x_2(t) = \dot{y}(t)$ 



**Dynamics** 

$$m\ddot{y} + b\dot{y} + ky = u \quad x_2(t) = \dot{y}(t)$$

 $x_1(t) = y(t)$ 

**State equation** 

$$\dot{x}_1 = x_2$$
  
$$\dot{x}_2 = -\frac{k}{m}x_1 - \frac{b}{m}x_2 + \frac{1}{m}u$$

**Output equation**  $y = x_1$ 



$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} u$$
$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$
$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$

#### **Correlation between State Space Representations and Transfer Functions**



$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$sX(s) - x(0) = AX(s) + BU(s)$$

$$Y(s) = CX(s) + DU(s)$$

$$(sI - A)X(s) = x(s) + BU(s)$$

$$Y(s) = CX(s) + DU(s)$$

$$X(s) = (sI - A)^{-1}BU(s)$$

$$Y(s) = CX(s) + DU(s)$$

#### **Correlation between State Space Representations and Transfer Functions**

$$\begin{array}{l}X(s) = (sI - A)^{-1}BU(s)\\Y(s) = CX(s) + DU(s)\end{array} \quad \frac{Y(s)}{U(s)} = C(sI - A)^{-1}B + D\end{array}$$

$$\frac{Y(s)}{U(s)} = \begin{bmatrix} 1 & 0 \end{bmatrix} \left\{ \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \right\}^{-1} \begin{bmatrix} 0 \\ 1/m \end{bmatrix} + 0$$

#### Transfer function

$$\frac{Y(s)}{U(s)} = \frac{1}{ms^2 + bs + k} <$$

#### **Time Domain Dynamics**

$$m\ddot{y} + b\dot{y} + ky = u$$

#### **Relation between State Space Representations and Transfer Functions**



#### **Relation between State Space Representations and Transfer Functions**

The dynamics of a linear system can be expressed in any of the forms

Differential equations
 Transfer functions
 State space representation

One has to note that given the TF for a system, state space representation is not unique. Different realizations can be performed.

State: The essence of past that influences the future. State is the smallest set of variables to describe the dynamics of a system

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} u$$

State Variables The dimension of the state vector is fixed for a given system

The dynamics of the system can uniquely be determined with the knowledge of  $x_1(t_0)$ ,  $x_2(t_0)$ and u(t) for  $t \ge t_0$ 

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} u$$

The state space is a space whose axes are the states. For the above example, axes are  $x_1$  axis and  $x_2$  axis.

In general we have a set of differential equations



$$\underline{\dot{x}} = \underline{f}(\underline{x}, \underline{u}, t)$$
$$\underline{y} = \underline{g}(\underline{x}, \underline{u}, t)$$

We linearize them and get

$$\underline{\dot{x}}(t) = A(t)\underline{x}(t) + B(t)\underline{u}(t)$$
$$\underline{y}(t) = C(t)\underline{x}(t) + D(t)\underline{u}(t)$$

The elements of the matrices may be time-varying

We simply dropped the underlines. Clearly the state will be a vector if its dimension is larger than one.



Or may be time invariant

#### **State Space Representation and Stability**

Assume you are given the system

$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$



The stability of this system can be determined by checking the eigenvalues of the matrix A



Those eigenvalues are the poles of the transfer function

$$\frac{Y(s)}{U(s)} = C(sI - A)^{-1}B + D$$

#### **State Space Representation and Stability**

$$\operatorname{eig}\{A\} = \{\lambda_1, \lambda_2, \lambda_3, \dots, \lambda_n\}$$

$$|\lambda I - A| = 0$$

If Re{ $\lambda_i$ }<0 for i=1,2,...,*n* Then the system is stable



If Re{ $\lambda_i$ }>0 for some i Then the system is unstable



If Re{ $\lambda_i$ }=0 for some i Then the system has poles on the imaginary axis

#### State Space Representation and Stability In summary...



$$\dot{x}_1 = x_2 - x_3 \qquad \qquad y = x_1$$
  
$$\dot{x}_2 = -x_1 + x_2 + x_3$$
  
$$\dot{x}_3 = ax_1 + x_2 - x_3 + u \qquad \qquad T(s) = \frac{Y(s)}{U(s)} = \frac{X_1(s)}{U(s)}$$

### Determine the range of a for stability

$$\dot{x}_{1} = x_{2} - x_{3}$$

$$\dot{x}_{2} = -x_{1} + x_{2} + x_{3}$$

$$\dot{x}_{3} = ax_{1} + x_{2} - x_{3} + u$$

$$T(s) = \frac{Y(s)}{U(s)} = \frac{X_{1}(s)}{U(s)}$$

$$sX_{1}(s) = X_{2}(s) - X_{3}(s)$$

$$sX_{2}(s) = -X_{1}(s) + X_{2}(s) + X_{3}(s)$$

$$sX_3(s) = aX_1(s) + X_2(s) - X_3(s) + U(s)$$

$$sX_{1}(s) = X_{2}(s) - X_{3}(s)$$
  

$$sX_{2}(s) = -X_{1}(s) + X_{2}(s) + X_{3}(s)$$
  

$$sX_{3}(s) = aX_{1}(s) + X_{2}(s) - X_{3}(s) + U(s)$$
  

$$X_{3}(s) = X_{2}(s) - sX_{1}(s)$$
  

$$X_{2}(s) = -\frac{s+1}{s-2}X_{1}(s)$$

$$X_{3}(s) = X_{2}(s) - sX_{1}(s)$$
$$X_{2}(s) = -\frac{s+1}{s-2}X_{1}(s)$$

$$X_3(s) = -\frac{s^2 - s + 1}{s - 2} X_1(s)$$

$$sX_{1}(s) = X_{2}(s) - X_{3}(s)$$

$$sX_{2}(s) = -X_{1}(s) + X_{2}(s) + X_{3}(s)$$

$$sX_{3}(s) = aX_{1}(s) + X_{2}(s) - X_{3}(s) + U(s)$$

$$X_{2}(s) = -\frac{s+1}{s-2}X_{1}(s)$$

$$X_{3}(s) = -\frac{s^{2}-s+1}{s-2}X_{1}(s)$$

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a} \begin{cases} s^3 & 1 & a-1 \\ s^2 & 0 & -2a \\ s^1 & & s^0 \end{cases}$$

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a}$$

$$s^{3} \qquad 1 \qquad a-1$$

$$s^{2} \qquad \varepsilon \qquad -2a$$

$$s^{1} \quad [\varepsilon(a-1)+2a]/\varepsilon \qquad 0$$

$$s^{0} \qquad -2a$$

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a}$$



$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a} \begin{bmatrix} 0 & 1 & -1 \\ -1 & 1 & 1 \\ a & 1 & -1 \end{bmatrix}$$

The system is unstable regardless of the value of *a*. In other words, A has at least one eigenvalue in the right half s-plane

# Can this system have poles on the imaginary axis?

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a}$$

# Assume the answer is yes... Then for $s=j\alpha$ the denominator must be zero, i.e.

$$(j\alpha)^3 + (a-1)(j\alpha) - 2a = 0$$
  
 $j(-\alpha^3 + (a-1)\alpha) - 2a = 0$ 

No value of *a* can lead to zero real and imaginary parts simultaneously

# Can this system have complex conjugate poles on the imaginary axis?

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a}$$

# The answer is no. Only one pole passes through the origin when a=0.

#### Watch now...

