

**WEEK 2: FUNDAMENTAL RELATIONS FOR THE FLOW THROUGH
AN ARBITRARY TURBOMACHINE**

**FUNDAMENTAL RELATIONS FOR THE FLOW THROUGH AN ARBITRARY
TURBOMACHINE:**

1-D Approximation

- The thickness of the blades are assumed to be zero.
- The number of blades is infinity, axisymmetric flow assumption.
- The flow is assumed to be uniform over each cross section.

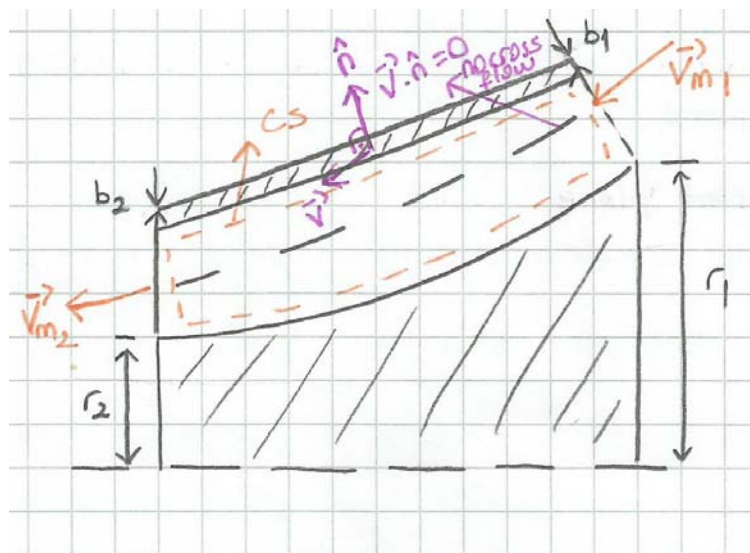


Figure1. Flow through meridional plane

a) Continuity Equation [1]:

The fluid flows in through area, A_1 of the control surface and flows out through area, A_2 of the control surface. No flow can take place through other surfaces of the control

volume, since they are formed by streamlines and $\vec{v} \cdot \vec{n} = 0$ on these surfaces. Therefore,

$$\int_{A_1} \rho_1 \cdot (\vec{v}_1 \cdot \vec{n}_1) \cdot dA + \int_{A_2} \rho_2 \cdot (\vec{v}_2 \cdot \vec{n}_2) \cdot dA = 0$$

1-D assumption assumes that areas A_1 and A_2 are perpendicular to velocities \vec{v}_1 and \vec{v}_2 , respectively; then

$$\begin{aligned} \vec{v}_1 \cdot \vec{n}_1 &= -v_{m_1} \\ \vec{v}_2 \cdot \vec{n}_2 &= +v_{m_2} \end{aligned}$$

Hence,

$$- \int_{A_1} \rho_1 \cdot \vec{v}_{m_1} \cdot dA + \int_{A_2} \rho_2 \cdot \vec{v}_{m_2} \cdot dA = 0$$

For a 1-D flow, the properties are uniform over each cross section, then

$$\dot{m} = \rho_1 \cdot v_{m_1} \cdot A_1 = \rho_2 \cdot v_{m_2} \cdot A_2$$

Noting that $A_1 = 2\pi \cdot r_1 \cdot b_1$ and $A_2 = 2\pi \cdot r_2 \cdot b_2$ with b_1 and b_2 are the width of the blades of the inlet and outlet, respectively.

$$\dot{m} = 2\pi \cdot r_1 \cdot b_1 \cdot v_{m_1} = 2\pi \cdot r_2 \cdot b_2 \cdot v_{m_2} = \text{constant}$$

b) Conservation of Angular Momentum [1]:

For a steady flow, the tangential component of the angular momentum is

$$T_Q = \int_{A_1} \rho_1 \cdot r_1 \cdot v_{Q_1} \cdot (\vec{v}_1 \cdot \vec{n}_1) \cdot dA + \int_{A_2} \rho_2 \cdot r_2 \cdot v_{Q_2} \cdot (\vec{v}_2 \cdot \vec{n}_2) \cdot dA$$

which can be rearranged to yield

$$T_Q = \int_{A_2} \rho_2 \cdot r_2 \cdot v_{Q_2} \cdot v_{m_2} \cdot dA - \int_{A_1} \rho_1 \cdot r_1 \cdot v_{Q_1} \cdot v_{Q_1} \cdot dA$$

For the uniform flow over each cross-section

$$T_Q = \rho_2 \cdot r_2 \cdot v_{Q_2} \cdot v_{m_2} \cdot A_2 - \rho_1 \cdot r_1 \cdot v_{Q_1} \cdot v_{m_1} \cdot A_1$$

Now, using the continuity equation;

$$T_Q = \dot{m} \cdot r_2 \cdot v_{Q_2} - \dot{m} \cdot r_1 \cdot v_{Q_1}$$

rearrange this equation;

$$T_Q = \dot{m} \cdot [r_2 \cdot v_{Q_2} - r_1 \cdot v_{Q_1}]$$

which is known Euler's turbine equation.

- The torque developed is equal to the rate of change of angular momentum
- The torque exerted in a fluid element in angular motion is equal to mass flow rate times the change in $r \cdot V_Q$. For a flow in which the torque is zero $r \cdot V_Q = \text{constant}$. This is called a free vortex flow.

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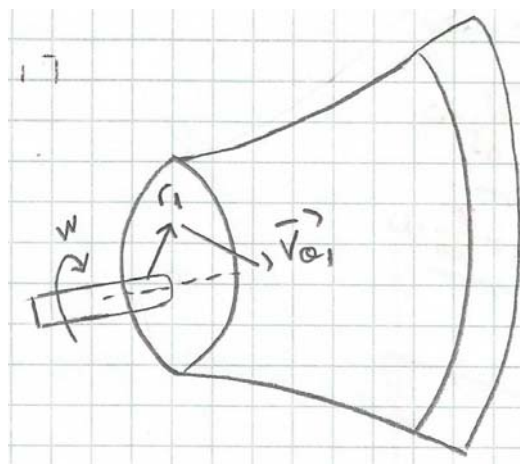


Figure 2: Swirl in a turbomachinery motor

The velocity component at the inlet and outlet of a pump and a turbine are shown, respectively.

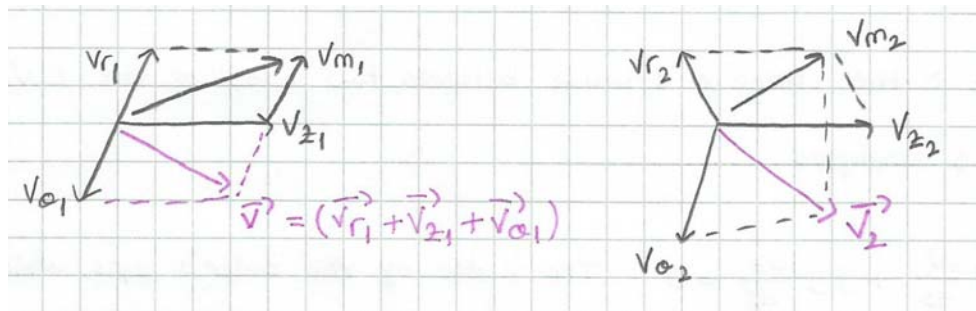


Figure 3. Velocity components

$$\dot{m} \cdot r_2 \cdot v_{Q_2}$$

$$\dot{m} \cdot r_1 \cdot v_{Q_1}$$

$$\dot{m} \cdot r_2 \cdot v_{Q_2} > \dot{m} \cdot r_1 \cdot v_{Q_1}$$

$$T_Q > 0(\text{pump})$$

$$\dot{m} \cdot r_2 \cdot v_{Q_2} < \dot{m} \cdot r_1 \cdot v_{Q_1}$$

$$T_Q < 0(\text{turbine})$$

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