



Ankara University  
Department of Geological Engineering



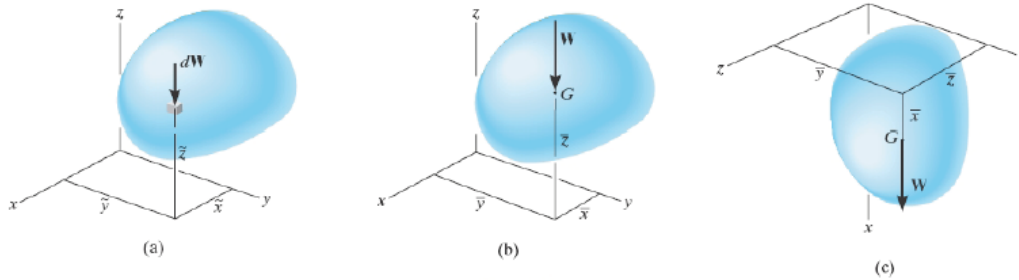
# GEO222 STATICS and STRENGTH of MATERIALS

Lecture Notes

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## Center of Gravity

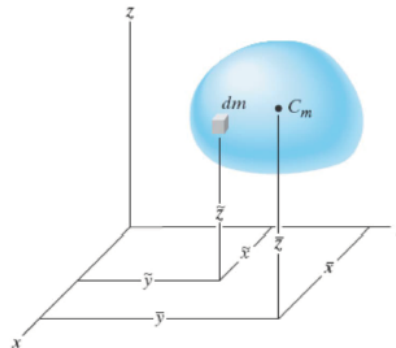
- Locates the resultant weight of a system of particles
- Consider system of n particles fixed within a region of space
- The weights of the particles can be replaced by a single (equivalent) resultant weight having defined point G of application



## Center Mass

- A rigid body is composed of an infinite number of particles
- Consider arbitrary particle having a weight of dW

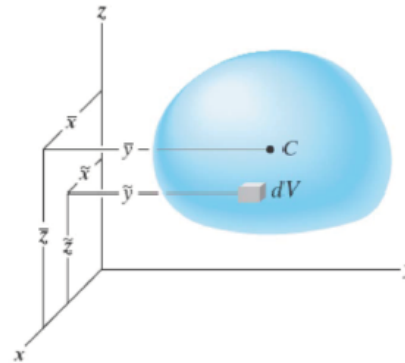
$$\bar{x} = \frac{\int \tilde{x} dW}{\int dW}; \bar{y} = \frac{\int \tilde{y} dW}{\int dW}; \bar{z} = \frac{\int \tilde{z} dW}{\int dW}$$



## Centroid of a Volume

- Consider an object subdivided into volume elements  $dV$ , for location of the centroid,

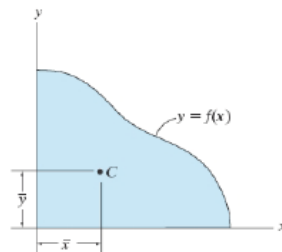
$$\bar{x} = \frac{\int \tilde{x} dV}{V}; \bar{y} = \frac{\int \tilde{y} dV}{V}; \bar{z} = \frac{\int \tilde{z} dV}{V}$$



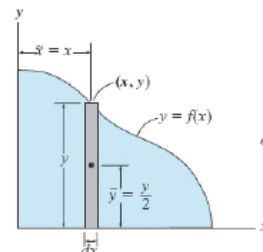
## Centroid of an Area

- For centroid for surface area of an object, such as plate and shell, subdivide the area into differential elements  $dA$

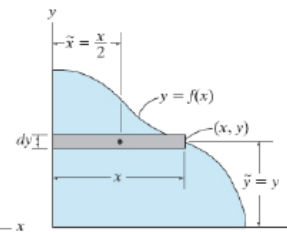
$$\bar{x} = \frac{\int \tilde{x} dA}{A}; \bar{y} = \frac{\int \tilde{y} dA}{A}; \bar{z} = \frac{\int \tilde{z} dA}{A}$$



(a)



(b)



(c)

**Example 21.** Please prove that the surface area of a sphere is  $A=4\pi R^2$  and the volume is  $V=4/3\pi R^3$

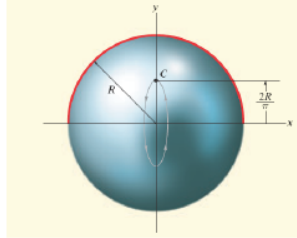
Surface Area

Generated by rotating semi-arc about the x axis

For centroid,  $\bar{r} = 2R / \pi$

For surface area,  $A = \theta \tilde{r} L;$

$$A = 2\pi \left( \frac{2R}{\pi} \right) \pi R = 4\pi R^2$$



Volume

Generated by rotating semicircular area about the x axis

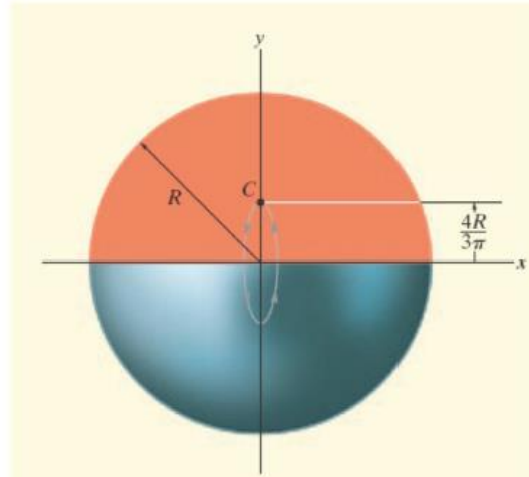
For centroid,

$$\bar{r} = 4R / 3\pi$$

For volume,

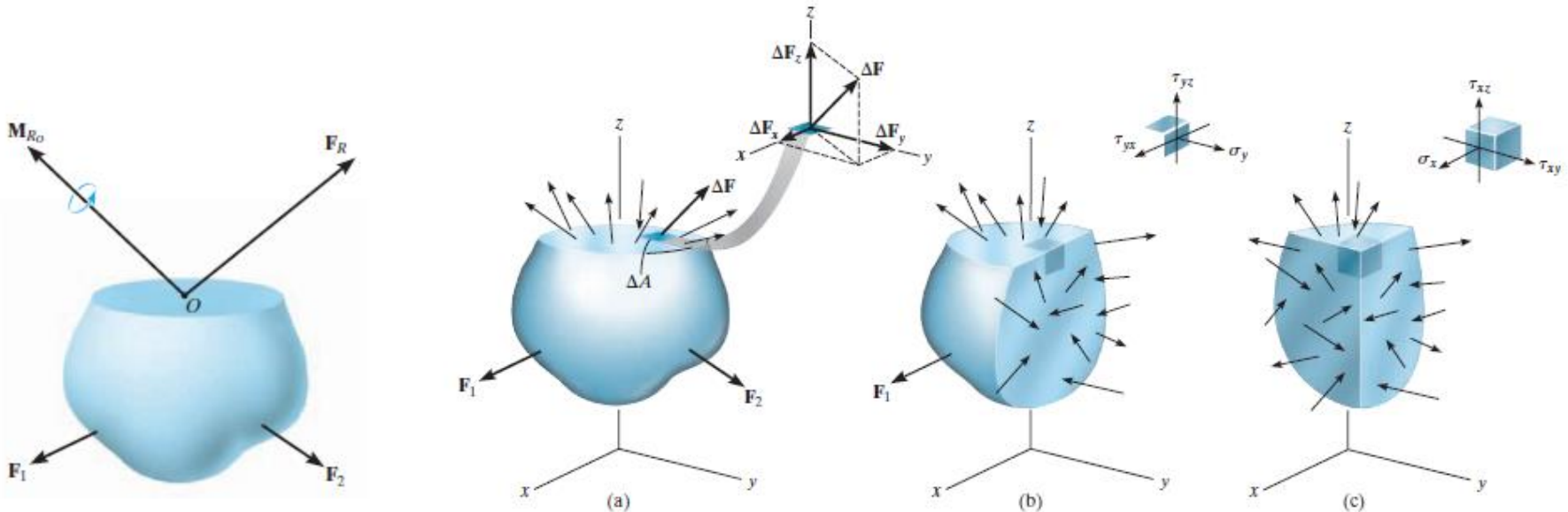
$$V = \theta \tilde{r} A;$$

$$V = 2\pi \left( \frac{4R}{3\pi} \right) \left( \frac{1}{2} \pi R^2 \right) = \frac{4}{3} \pi R^3$$



## Stress Concept

Based on the force and moment acting at a specified point  $O$  on the sectioned area of the body, (Fig.a) represents the resultant effects of the actual *distribution of loading* acting over the sectioned area, Fig.b. Considering the sectioned area to be subdivided into small areas, such as  $\Delta A$  (Fig.b). As we reduce  $\Delta A$  to a smaller and smaller size, we must make two assumptions regarding the properties of the material. We will consider the material to be **continuous**, that is, to consist of a *continuum* or uniform distribution of matter having no voids. A typical finite yet very small force  $\Delta F$  acting on  $\Delta A$  is shown in Fig. a. This force, like all the others, will have a unique direction, but for further discussion we will replace it by its *three components*, namely,  $\Delta F_x$ ,  $\Delta F_y$  and  $\Delta F_z$ . As  $\Delta A$  approaches zero, so do  $\Delta F$  and its components; however, the quotient of the force and area will, in general, approach a finite limit. **This quotient is called stress, and as noted, it describes the intensity of the internal force acting on a specific plane (area) passing through a point** (Hibbeler, 2010).



## Normal Stress

The *intensity* of the force acting normal to  $\Delta A$  is defined as the **normal stress**, ( $\sigma$ ). Since  $DF_z$  is normal to the area then;

$$\sigma_z = \lim_{\Delta A \rightarrow 0} \frac{\Delta F_z}{\Delta A}$$

If the normal force or stress “pulls”, it is referred to as *tensile stress*, whereas if it “pushes” on it is called *compressive stress*.

## Shear Stress

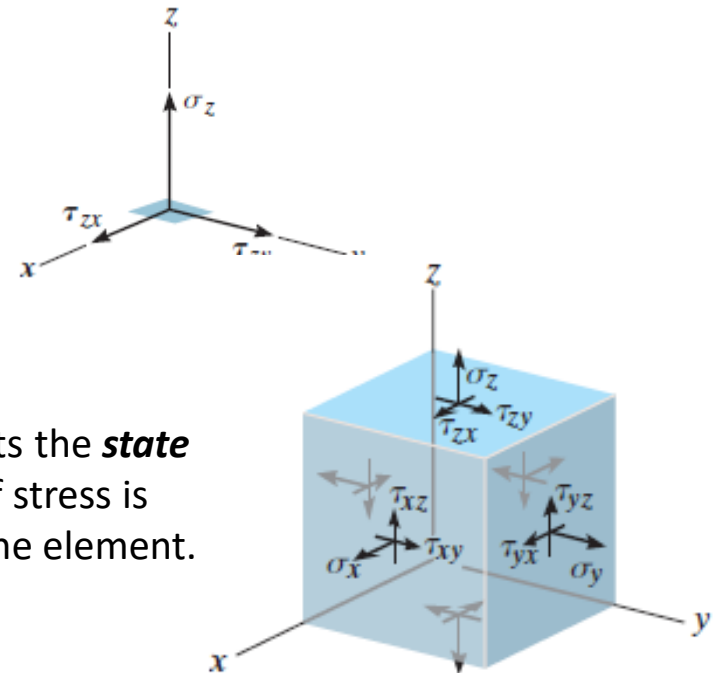
The intensity of force acting tangent to  $\Delta A$  is called the **shear stress**, ( $\tau$ ). Here we have shear stress components,

$$\tau_{zx} = \lim_{\Delta A \rightarrow 0} \frac{\Delta F_x}{\Delta A}$$

$$\tau_{zy} = \lim_{\Delta A \rightarrow 0} \frac{\Delta F_y}{\Delta A}$$

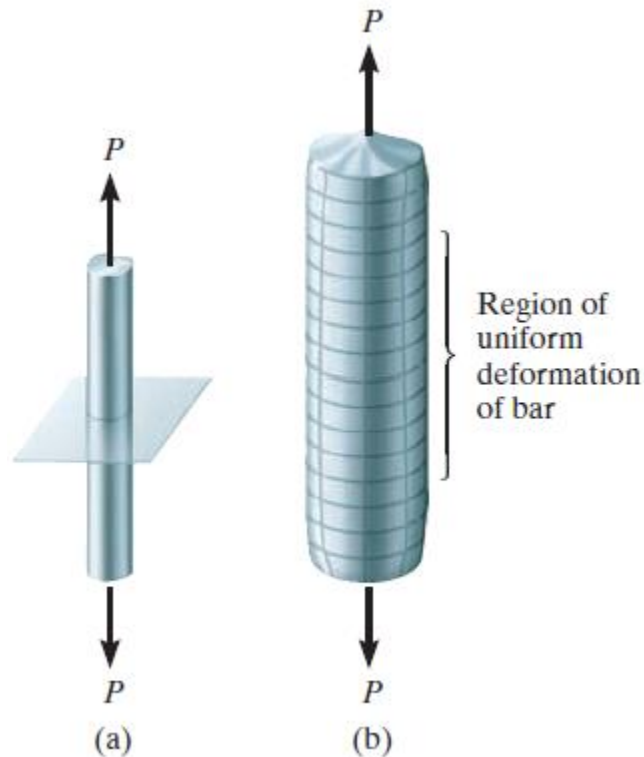
## General State of Stress

If we “cut out” a cubic volume element of material that represents the **state of stress** acting around the chosen point in the body. This state of stress is then characterized by three components acting on each face of the element.



## Average Normal Stress in an Axially Loaded Bar

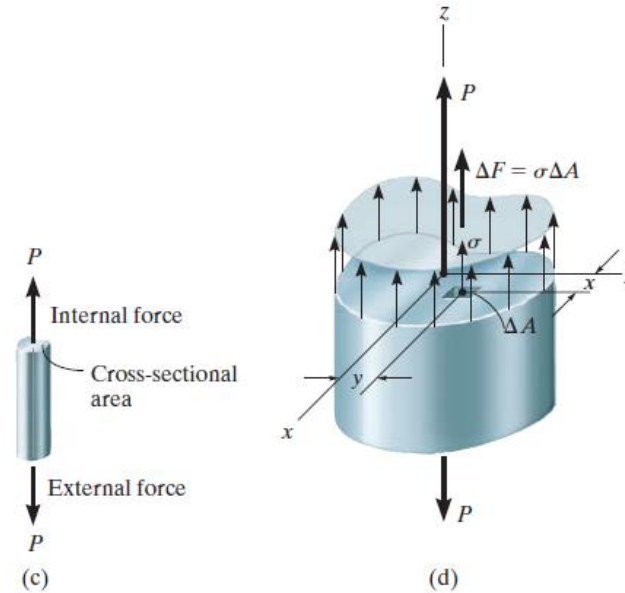
In this section we will determine the average stress distribution acting on the cross-sectional area of an axially loaded bar (Fig. *a*). This bar is **prismatic** since all cross sections are the same throughout its length. When the load “*P*” is applied to the bar through the centroid of its cross-sectional area, then the bar will deform uniformly throughout the central region of its length (Fig. *b*) provided the material of the bar is both homogeneous and isotropic. **Homogeneous material** has the same physical and mechanical properties throughout its volume, and **isotropic material** has these same properties in all directions. Many engineering materials may be approximated as being both homogeneous and isotropic as assumed here.



(Hibbeler, 2010)

## Average Normal Stress Distribution

If we pass a section through the bar, and separate it into two parts, then equilibrium requires the resultant normal force at the section to be  $P$ , (Fig. c.) Due to the *uniform* deformation of the material, it is necessary that the cross section be subjected to a *constant normal stress distribution* (Fig. d)



As a result, each small area  $\Delta A$  on the cross section is subjected to a force  $\Delta F = \sigma \Delta A$ , and the *sum* of these forces “ $F = \sigma \Delta A$ ” acting over the entire cross-sectional area must be equivalent to the internal resultant force  $\mathbf{P}$  at the section.

$$+\uparrow F_{Rz} = \Sigma F_z;$$

$$\int dF = \int_A \sigma dA$$

$$P = \sigma A$$

$$\sigma = \frac{P}{A}$$

$\sigma$  = average normal stress at any point on the cross-sectional area

$P$  = *internal resultant normal force*, which acts through the *centroid* of the cross-sectional area.  $P$  is determined using the method of sections and the equations of equilibrium

$A$  = cross-sectional area of the bar where  $\sigma$  is determined