

| Typical packing efficiencies |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| System | Pressure $\mathbf{k P a}$ | Column dia, $m$ | Packing |  | $\begin{aligned} & \text { HTU } \\ & \mathbf{m} \end{aligned}$ | $\begin{aligned} & \text { HETP } \\ & \mathbf{m} \end{aligned}$ |
|  |  |  | type | size, mm |  |  |
| Absorption |  |  |  |  |  |  |
| Hydrocarbons | 6000 | 0.9 | Pall | 50 |  | 0.85 |
| $\mathrm{NH}_{3}$-Air- $\mathrm{H}_{2} \mathrm{O}$ | 101 | - | Berl | 50 | 0.50 |  |
| Air-water | 101 | - | Berl | 50 | 0.50 |  |
| Acetone-water | 101 | 0.6 | Pall | 50 |  | 0.75 |
| Distillation |  |  |  |  |  |  |
| Pentane-propane | 101 | 0.46 | Pall | 25 |  | 0.46 |
| IPA-water | 101 | 0.46 | Int. | 25 | 0.75 | 0.50 |
| Methanol-water | 101 | 0.41 | Pall | 25 | 0.52 |  |
|  | 101 | 0.20 | Int. | 25 |  | 0.46 |
| Acetone-water | 101 | 0.46 | Pall | 25 |  | 0.37 |
|  | 101 | 0.36 | Int. | 25 |  | 0.46 |
| Formic acid-water | 101 | 0.91 | Pall | 50 |  | 0.45 |
| Acetone-water | 101 | 0.38 | Pall | 38 | 0.55 | 0.45 |
|  | 101 | 0.38 | Int. | 50 | 0.50 | 0.45 |
|  | 101 | 1.07 | Int. | 38 |  | 1.22 |
| MEK-toluene | 101 | 0.38 | Pall | 25 | 0.29 | 0.35 |
|  | 101 | 0.38 | Int. | 25 | 0.27 | 0.23 |
|  | 101 | 0.38 | Berl | 25 | 0.31 | 0.31 |
| Pall $=$ Pall rings, Berl $=$ Berl saddles, Int. $=I N T A L O X ~$ saddles |  |  |  |  |  |  |

## Cornell Correlation

Equations and figures are given for a range of sizes of Raschig rings and Berl saddles.

$$
\begin{gathered}
\mathbf{H}_{G}=0.011 \psi_{h}(S c)_{v}^{0.5}\left(\frac{D_{c}}{0.305}\right)^{1.11}\left(\frac{Z}{3.05}\right)^{0.33} /\left(L_{k}^{*} f_{1} f_{2} f_{3}\right)^{0.5} \\
\mathbf{H}_{L}=0.305 \phi_{h}(S c)_{L}^{0.5} K_{3}\left(\frac{Z}{3.05}\right)^{0.15}
\end{gathered}
$$

## Onda's Method

$$
\begin{aligned}
k_{L}\left(\frac{\rho_{L}}{\mu_{L} g}\right)^{1 / 3} & =0.0051\left(\frac{L_{w}^{*}}{a_{w} \mu_{L}}\right)^{2 / 3}\left(\frac{\mu_{L}}{\rho_{L} D_{L}}\right)^{-1 / 2}\left(a d_{p}\right)^{0.4} \\
\frac{k_{G}}{a} \frac{R T}{D_{v}} & =K_{5}\left(\frac{V_{w}^{*}}{a \mu_{v}}\right)^{0.7}\left(\frac{\mu_{v}}{\rho_{v} D_{v}}\right)^{1 / 3}\left(a d_{p}\right)^{-2.0}
\end{aligned}
$$

- It consists of useful correlations for the film mass-transfer coefficients $\mathrm{k}_{\mathrm{G}}$ and $\mathrm{k}_{\mathrm{L}}$ and the effective wetted area of the packing $a_{w}$, which can be used to calculate $\mathbf{H}_{\mathbf{G}}$ and $\mathbf{H}_{\mathbf{L}}$.
- 

$$
\begin{aligned}
\mathbf{H}_{G} & =\frac{G_{m}}{k_{G} a_{w} P} \\
\mathbf{H}_{L} & =\frac{L_{m}}{k_{L} a_{w} C_{t}}
\end{aligned}
$$

## COLUMN DIAMETER (CAPACITY)

The capacity of a packed column is determined by its cross-sectional area.

Normally, the column will be designed to operate at the highest economical pressure drop, to ensure good liquid and gas distribution.

For random packings the pressure drop will not normally exceed 80 mm of water per meter of packing height.

- Generalized pressure drop correlation


$$
K_{4}=\frac{13.1\left(V_{w}^{*}\right)^{2} F_{p}\left(\frac{\mu_{L}}{\rho_{L}}\right)^{0.1}}{\rho_{v}\left(\rho_{L}-\rho_{v}\right)}
$$

$V_{w}^{*}=$ gas mass flow-rate per unit column cross-sectional area, $\mathrm{kg} / \mathrm{m}^{2} \mathrm{~s}$
$F_{p}=$ packing factor, characteristic of the size and type of packing.
$\mu_{L}=$ liquid viscosity, $\mathrm{Ns} / \mathrm{m}^{2}$
$\rho_{L}, \rho_{v}=$ liquid and vapour densities, $\mathrm{kg} / \mathrm{m}^{3}$

## REFERENCES

1. Sinnot, R.K. 1999, Coulson's \& Richardson's Chemical Engineering, Volume 6, Chemical Engineering Design, ButterWorth Heinemann, Oxford.
2. Turton R., Bailie R.C., Whitin W.C., Shaeiwitz J.A. 1998, Analysis, Synthesis and Design of Chemical Processes, Prentice Hall, New Jersey.
