



# BME 202 Electronics

## Lecture 13: BJT and JFET Frequency Response

# General Frequency Considerations

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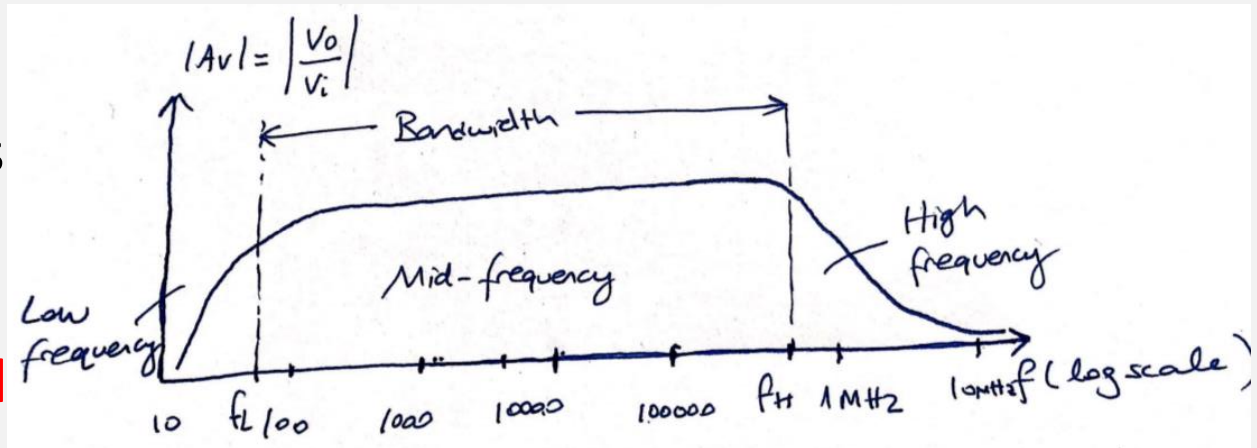
**Frequency Response:** The frequency range in which an amplifier will operate with negligible effects from capacitors and device internal capacitances; often called the **mid-range**.

- At frequencies **below** mid-range, the **coupling and bypass capacitors** lower the gain.
- At frequencies **above** mid-range, **stray capacitances** associated with the active device lower the gain.
- Also, cascading amplifiers limits the gain at high and low frequencies.

# Bode Plot

A **Bode plot** illustrates the frequency response of an amplifier.

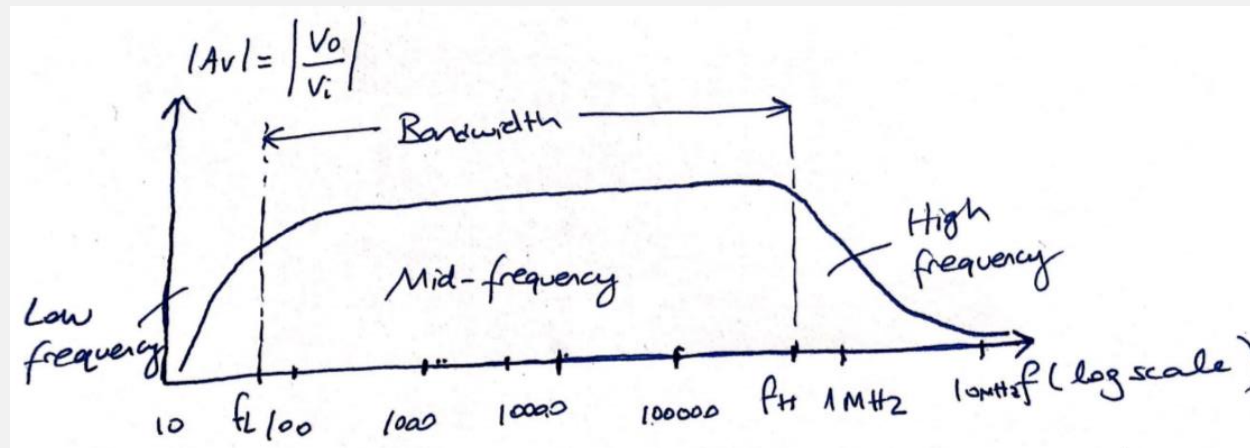
The **horizontal scale** indicates the frequency (in Hz) and the **vertical scale** indicates the gain (in dB).



# Cutoff Frequencies

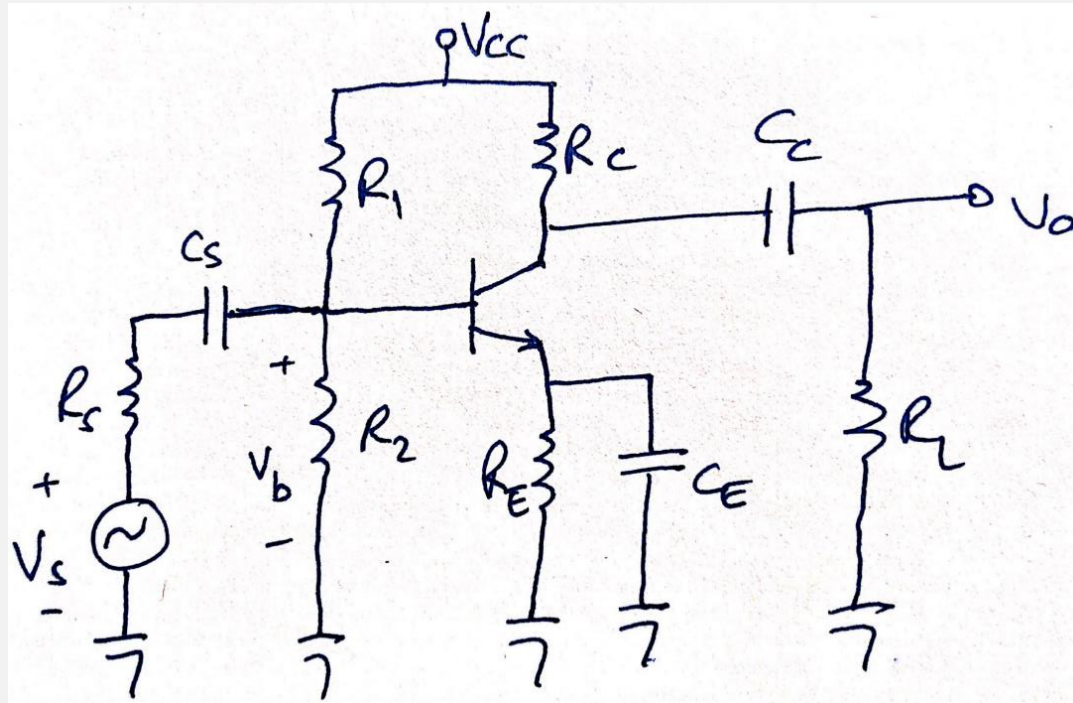
The mid-range of an amplifier is called the **bandwidth** of the amplifier.

The bandwidth is defined by the lower and upper cutoff frequencies.



**Cutoff frequency** – any frequency at which the gain has dropped by 3 dB from its mid-range value

# BJT Amplifier Low-Frequency Response



At **low frequencies**, the reactance of the **coupling capacitors** ( $C_S$ ,  $C_C$ ) and the **bypass capacitor** ( $C_E$ ) affect the circuit impedances.

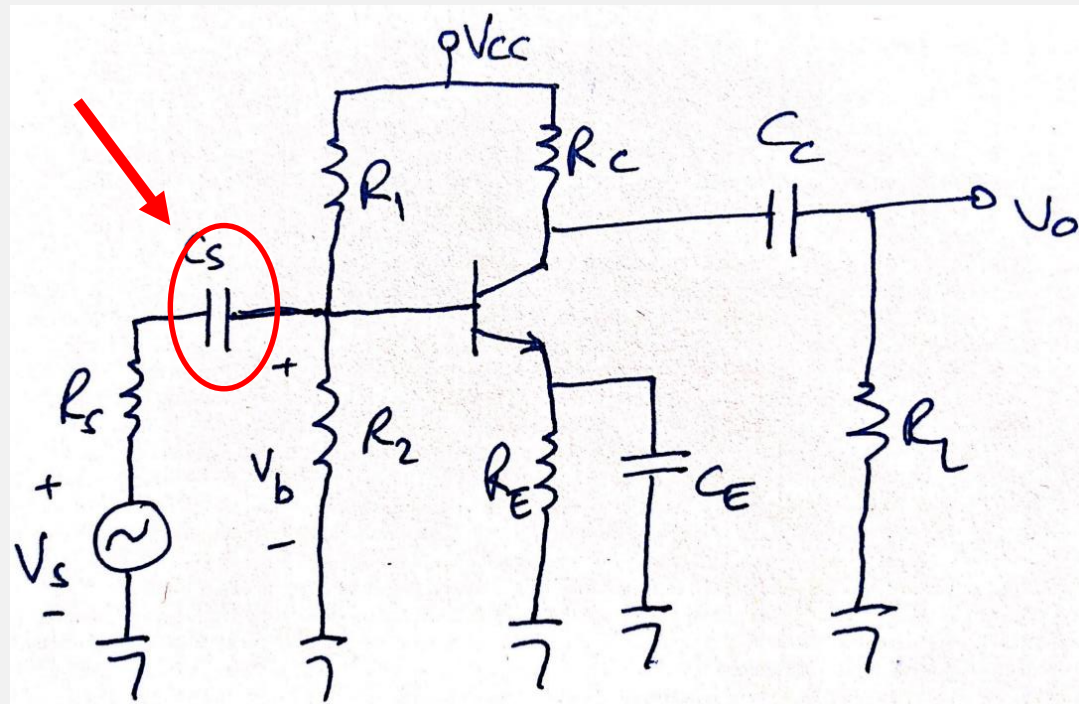
# Coupling Capacitor ( $C_s$ )

The cutoff frequency due to  $C_s$  can be calculated using

$$f_{Ls} = \frac{1}{2\pi(R_s + R_i)C_s}$$

where

$$R_i = R_1 // R_2 // \beta R_e$$



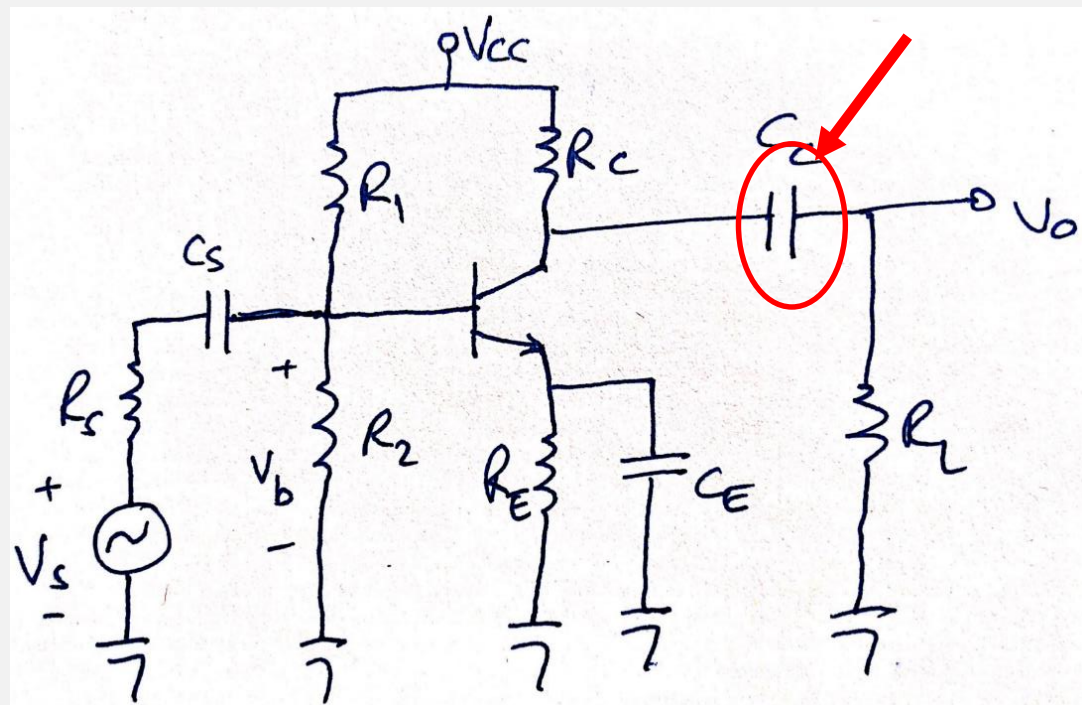
# Coupling Capacitor ( $C_c$ )

The cutoff frequency due to  $C_c$  can be calculated using

$$f_{LC} = \frac{1}{2\pi(R_o + R_L)C_c}$$

where

$$R_o = R_C // r_o$$





# Bypass Capacitor ( $C_E$ )

The cutoff frequency due to  $C_E$  can be calculated using

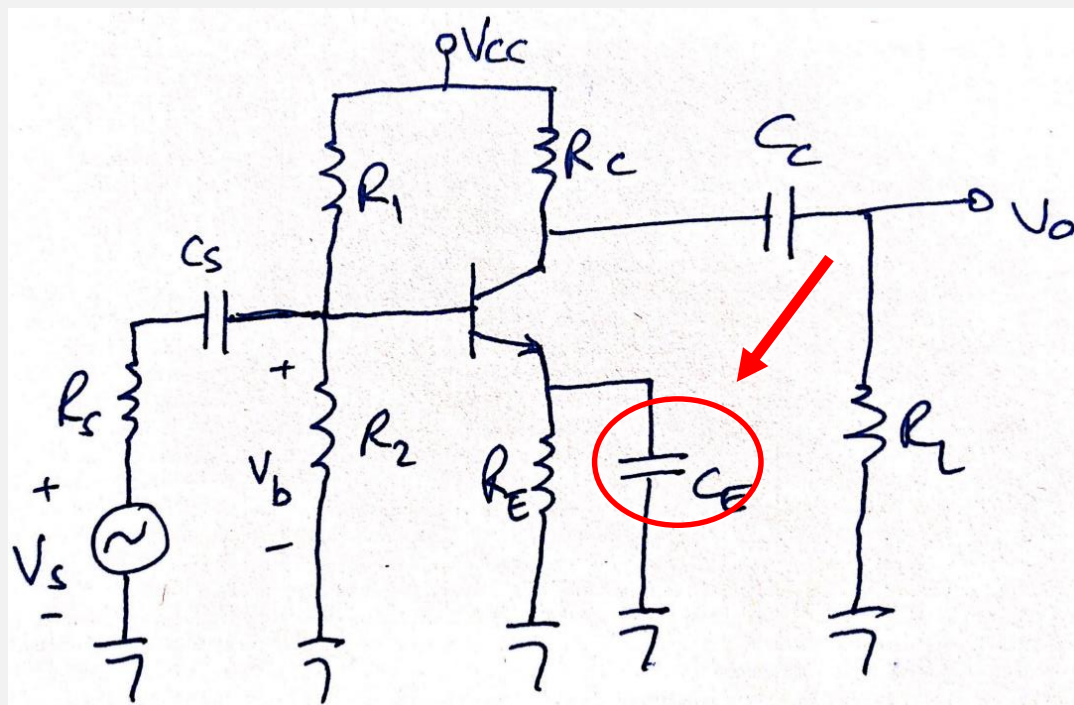
$$f_{LE} = \frac{1}{2\pi R_e C_E}$$

where

$$R_e = R_E // \left( \frac{R'_s}{\beta} + r_e \right)$$

and

$$R'_s = R_s // R_1 // R_2$$







# BJT Amplifier Low-Frequency Response

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The Bode plot indicates that each capacitor may have a different cutoff frequency.

It is the device that has the *highest* lower cutoff frequency ( $f_L$ ) that dominates the overall low-frequency response of the amplifier.



# Roll-Off of Gain in the Bode Plot

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- The Bode plot not only indicates the cutoff frequencies of the various capacitors, it also indicates the amount of attenuation (loss in gain) at these frequencies.
- The rate of attenuation is sometimes referred to as **roll-off**.

The roll-off is measured in **dB-per-octave** or **dB-per-decade**.

# Roll-Off Rate (dB/Decade)

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**-dB/decade** refers to the attenuation for every 10-fold change in frequency.

For attenuations at the low-frequency end, it refers to the loss in gain from the lower cutoff frequency to a frequency that is one-tenth the cutoff value.

$$f_{LS} = 9\text{kHz gain is } 0\text{dB}$$

$$f_{LS}/10 = .9\text{kHz gain is } -20\text{dB}$$

Thus the roll-off is **-20dB/decade**

# Roll-Off Rate (-dB/Octave)

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**-dB/octave** refers to the attenuation for every 2-fold change in frequency.

For attenuations at the low-frequency end, it refers to the loss in gain from the lower cutoff frequency to a frequency one-half the cutoff value.

This is a little difficult to see on this graph because the horizontal scale is a logarithmic scale.

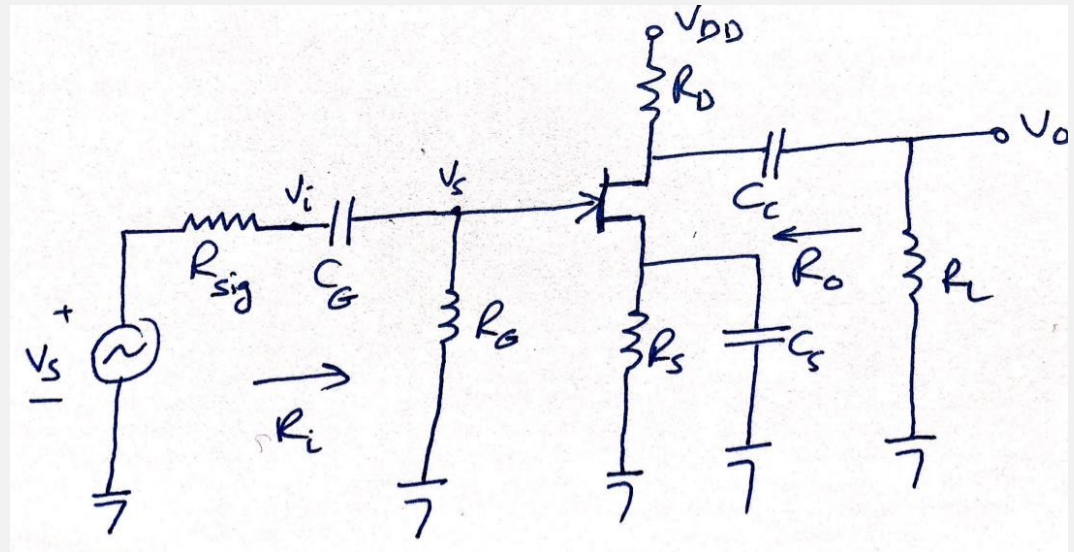
$f_{LS} = 9\text{kHz}$  gain is 0dB

$f_{LS} / 2 = 4.5\text{kHz}$  gain is -6dB

Therefore the roll-off is 6dB/octave.

# FET Amplifier Low-Frequency Response

At low frequencies, the reactances of the coupling capacitors ( $C_G$ ,  $C_C$ ) and the bypass capacitor ( $C_S$ ) affect the circuit impedances.



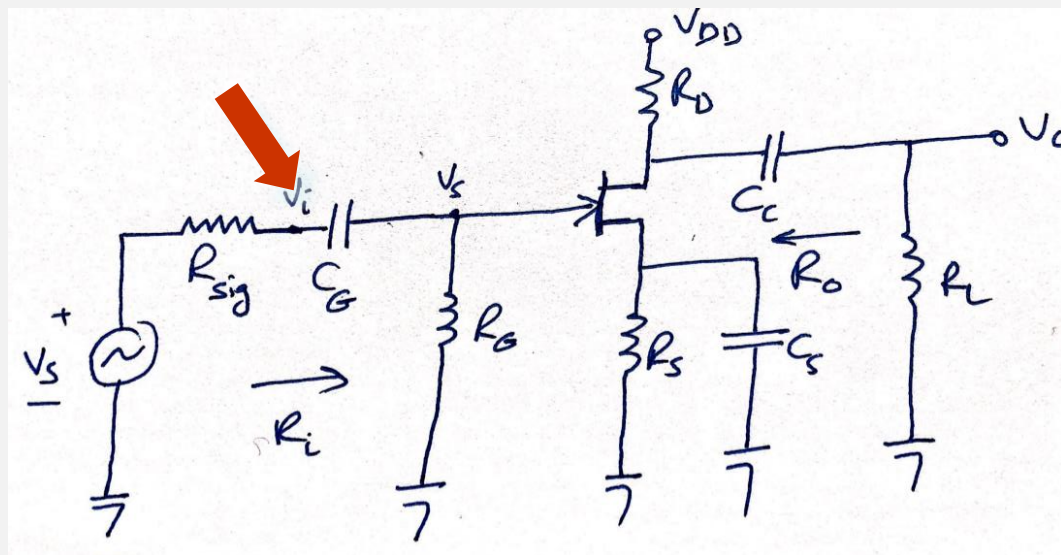
# Coupling Capacitor (CG)

The cutoff frequency due to  $C_G$  can be calculated with

$$f_{LC} = \frac{1}{2\pi(R_{sig} + R_i)C_G}$$

where

$$R_i = R_G$$





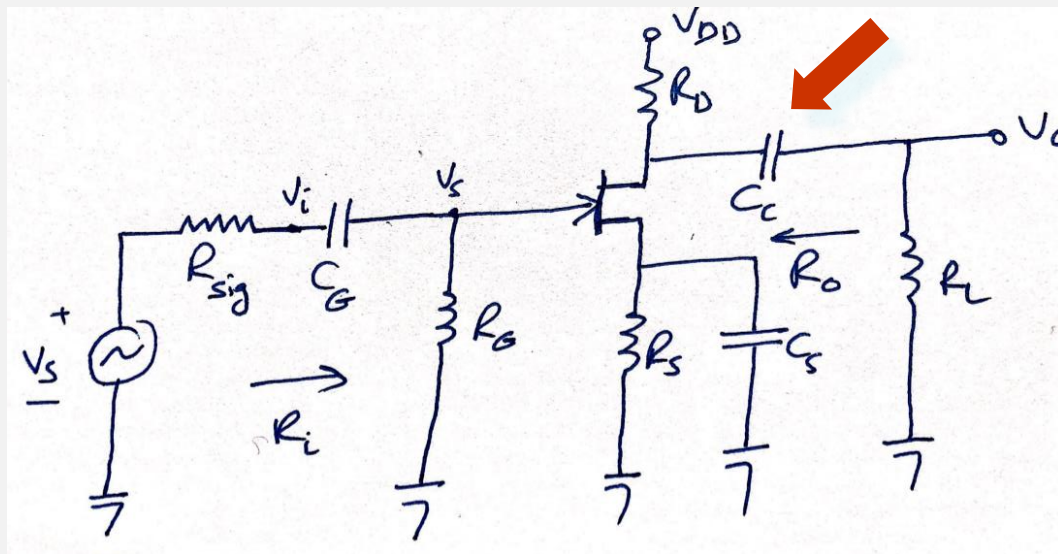
# Coupling Capacitor (CC)

The cutoff frequency due to  $C_C$  can be calculated with

$$f_{LC} = \frac{1}{2\pi(R_o + R_L)C_C}$$

where

$$R_o = R_D \parallel r_d$$



# Bypass Capacitor (CS)

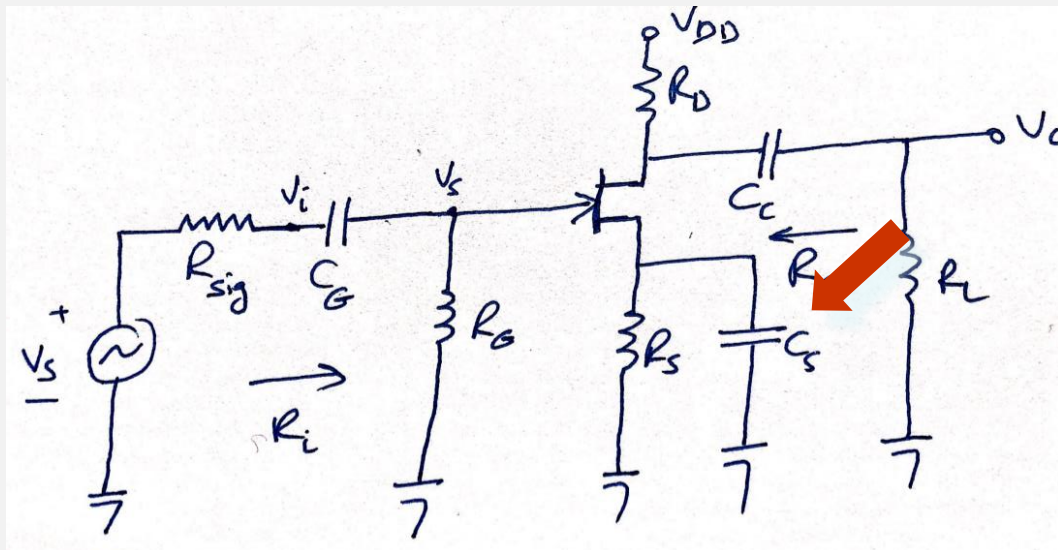
## Bypass Capacitor ( $C_S$ )

The cutoff frequency due to  $C_S$  can be calculated with

$$f_{LS} = \frac{1}{2\pi R_{eq} C_S}$$

where

$$R_{eq} = R_S \parallel \frac{1}{g_m} \Big|_{r_d \approx \infty \Omega}$$



# FET Amplifier Low-Frequency Response

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The Bode plot indicates that each capacitor may have a different cutoff frequency.

The capacitor that has the *highest* lower cutoff frequency ( $f_L$ ) is closest to the actual cutoff frequency of the amplifier.

# Miller Capacitance

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Any  $p-n$  junction can develop capacitance. This capacitance becomes noticeable across:

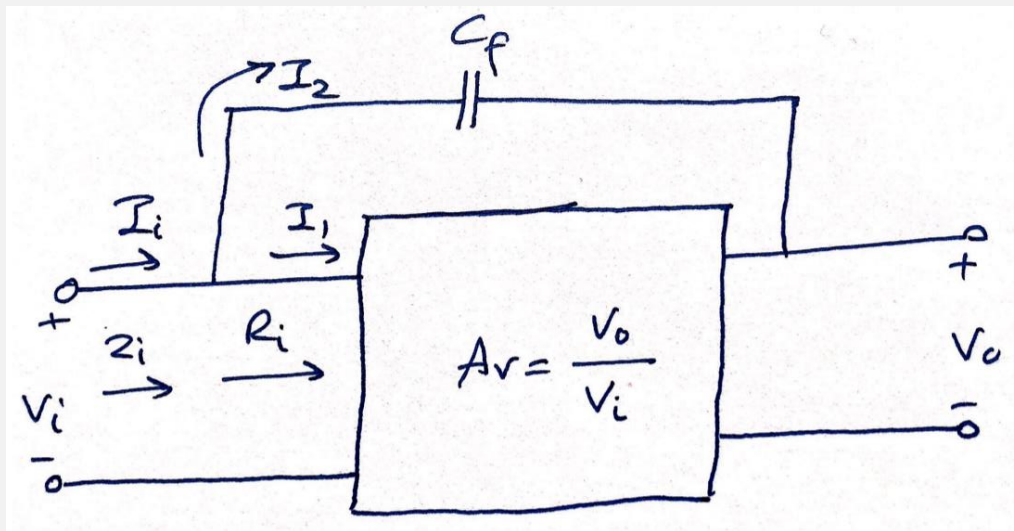
- The BJT base-collector junction in a common-emitter amplifier operating at high frequencies
- The FET gate-drain junction in a common-source amplifier at high frequencies

These capacitances are represented as separate input and output capacitances, called the **Miller capacitances**.

# Miller Input Capacitance ( $C_{MI}$ )

$$C_{Mi} = (1 - A_v)C_f$$

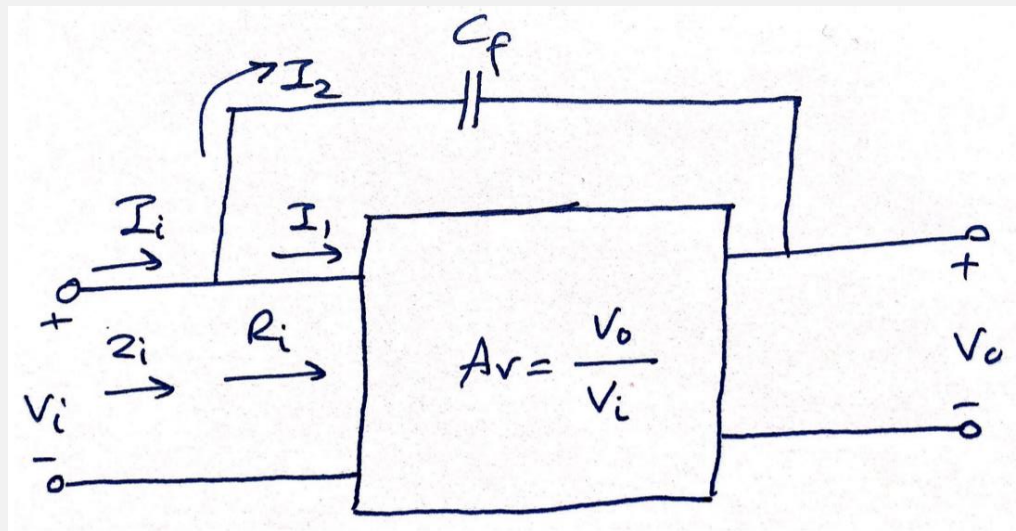
Note that the amount of Miller capacitance is dependent on inter-electrode capacitance from input to output ( $C_f$ ) and the gain ( $A_v$ ).



# Miller Output Capacitance ( $C_{MO}$ )

If the gain ( $A_v$ ) is considerably greater than 1, then

$$C_{MO} \cong C_f$$





# BJT Amplifier High-Frequency Response

Capacitances that affect the high-frequency response are

Junction capacitances

$$C_{be}, C_{bc}, C_{ce}$$

Wiring capacitances

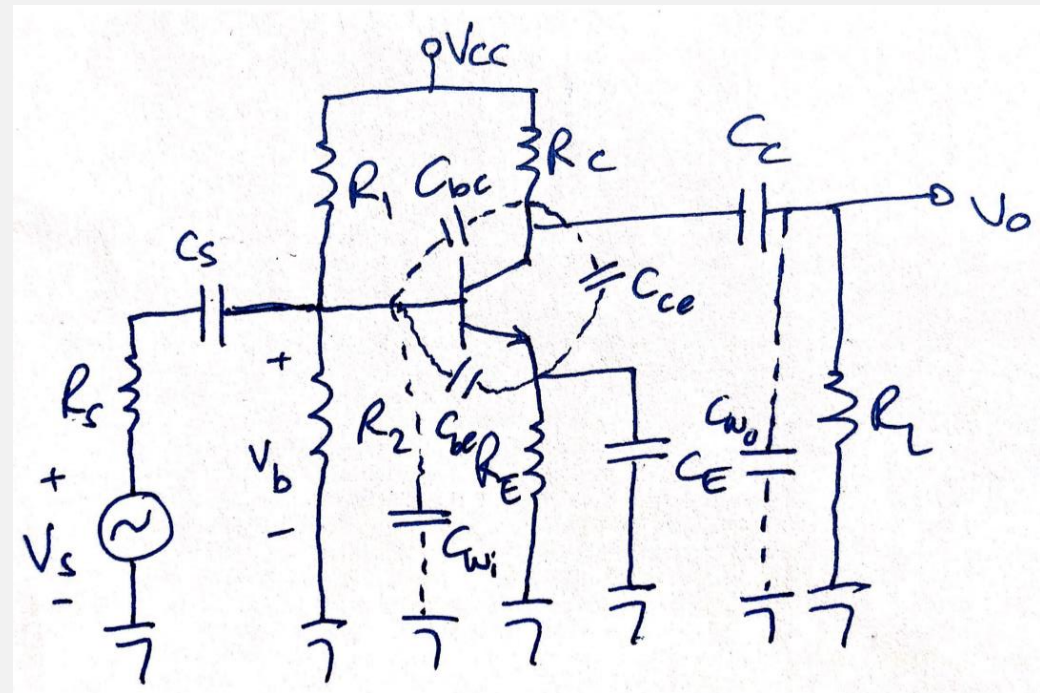
$$C_{wi}, C_{wo}$$

Coupling capacitors

$$C_S, C_C$$

Bypass capacitor

$$C_E$$



# Input High-Frequency Cutoff (f<sub>Hi</sub>)

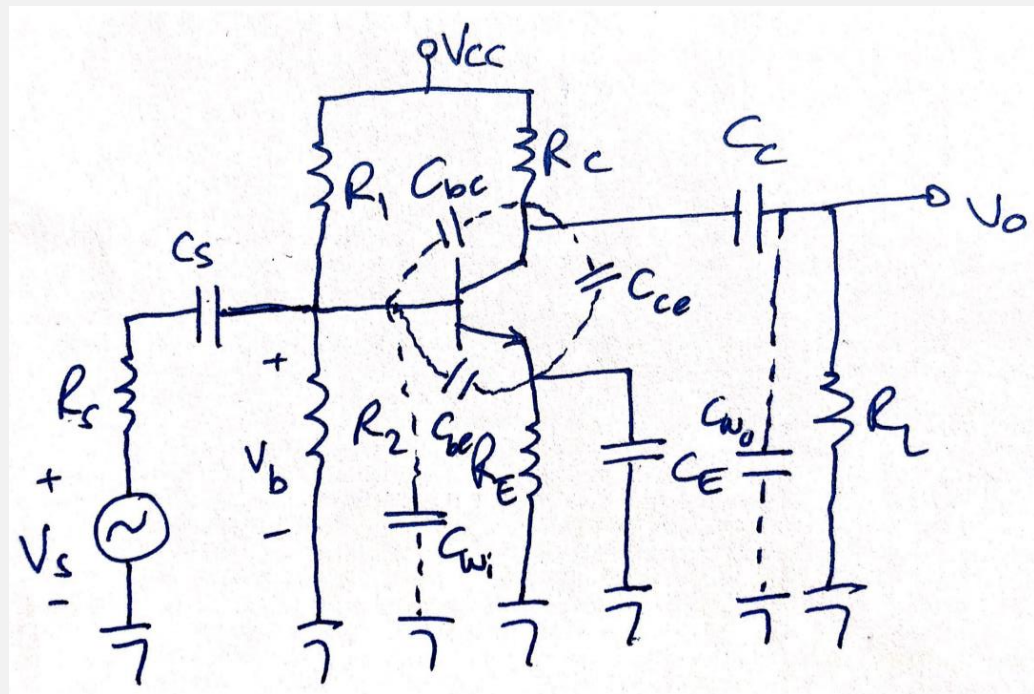
$$f_{Hi} = \frac{1}{2\pi R_{Thi} C_i}$$

where

$$R_{Thi} = R_s \parallel R_1 \parallel R_2 \parallel R_i$$

and

$$\begin{aligned} C_i &= C_{Wi} + C_{be} + C_{Mi} \\ &= C_{Wi} + C_{be} + (1 - A_v) C_{bc} \end{aligned}$$



# Output High-Frequency Cutoff (f<sub>Ho</sub>)

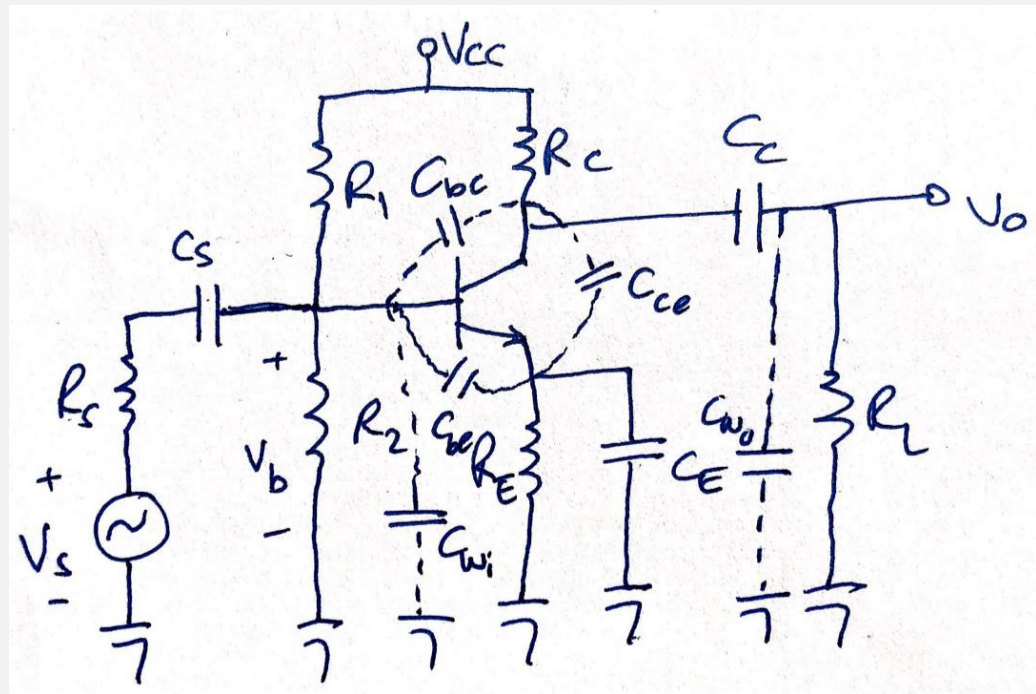
$$f_{Ho} = \frac{1}{2\pi R_{Tho} C_o}$$

where

$$R_{Tho} = R_C \parallel R_L \parallel r_o$$

and

$$C_o = C_{Wo} + C_{ce} + C_{Mo}$$



# FET Amplifier High-Frequency Response

Capacitances that affect the high-frequency response:

Junction capacitances

$$C_{gs}, C_{gd}, C_{ds}$$

Wiring capacitances

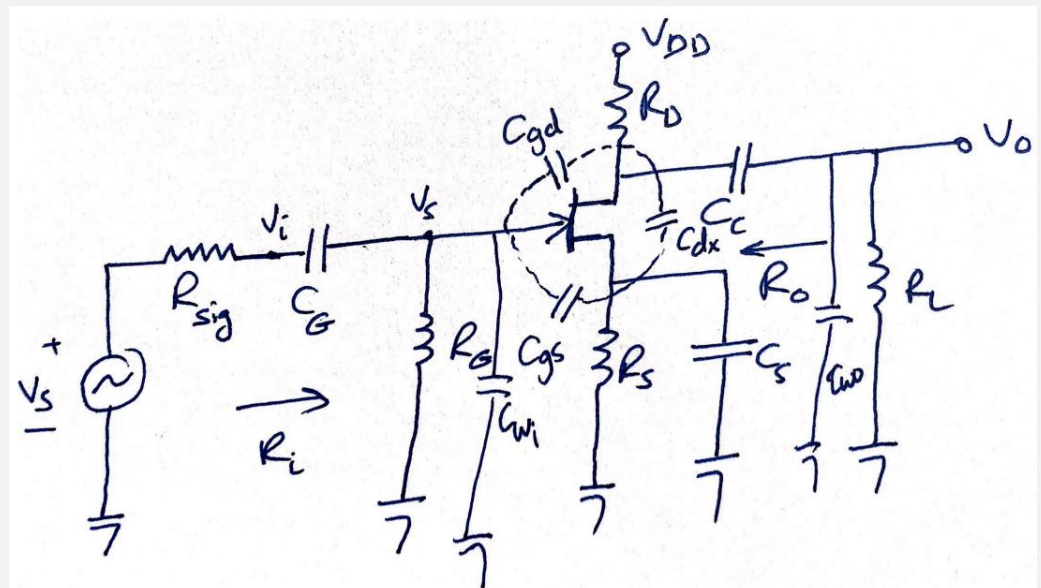
$$C_{wi}, C_{wo}$$

Coupling capacitors

$$C_G, C_C$$

Bypass capacitor

$$C_S$$



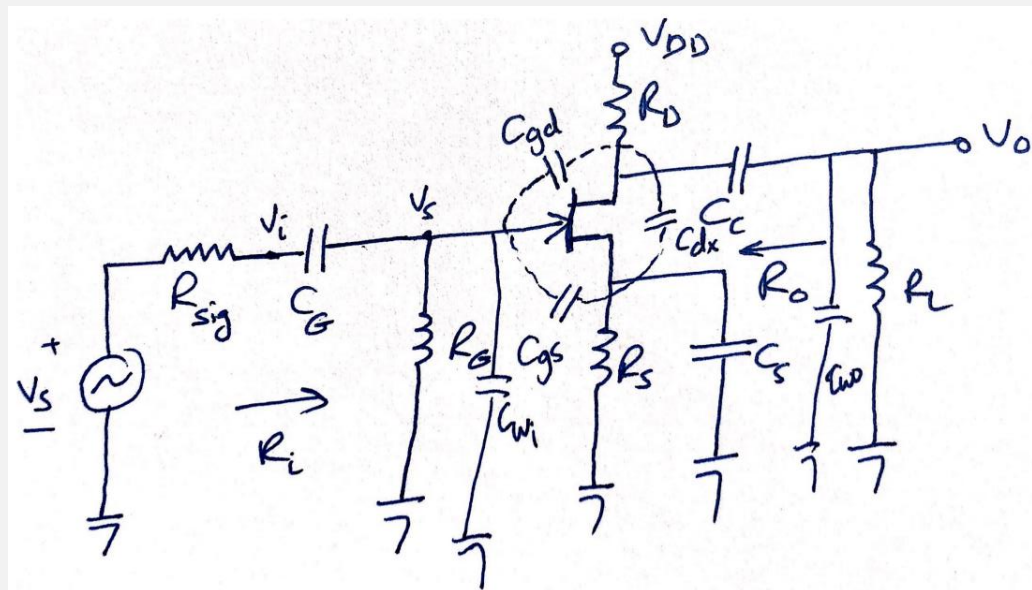
# Input High-Frequency Cutoff ( $f_{Hi}$ )

$$f_{Hi} = \frac{1}{2\pi R_{Thi} C_i}$$

$$C_i = C_{Wi} + C_{gs} + C_{Mi}$$

$$C_{Mi} = (1 - A_V) C_{gd}$$

$$R_{Thi} = R_{sig} \parallel R_G$$





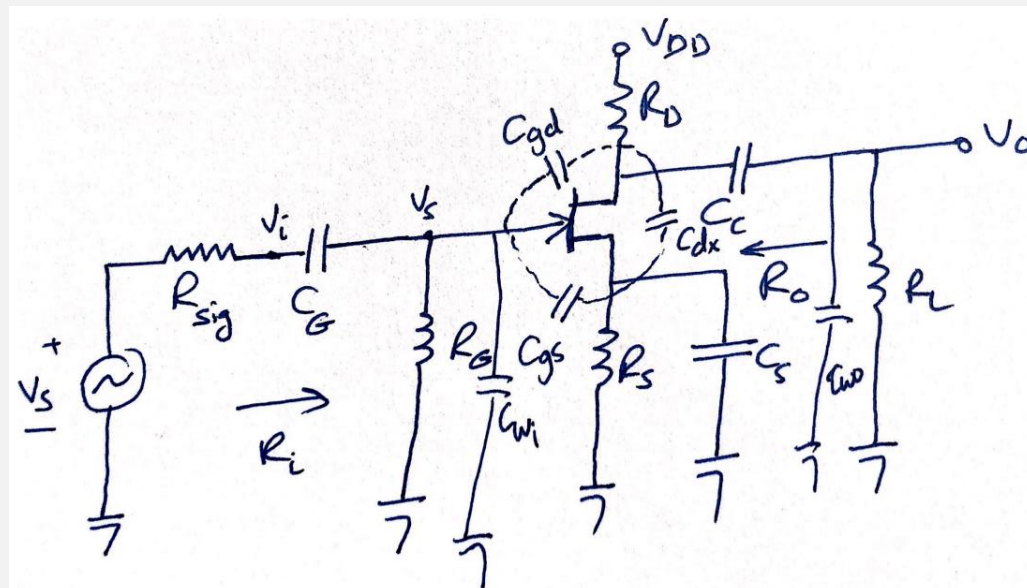
# Output High-Frequency Cutoff ( $f_{Ho}$ )

$$f_{Ho} = \frac{1}{2\pi R_{Tho} C_o}$$

$$C_o = C_{Wo} + C_{ds} + C_{Mo}$$

$$C_{Mo} = \left(1 - \frac{1}{A_v}\right) C_{gd}$$

$$R_{Tho} = R_D || R_L || r_d$$



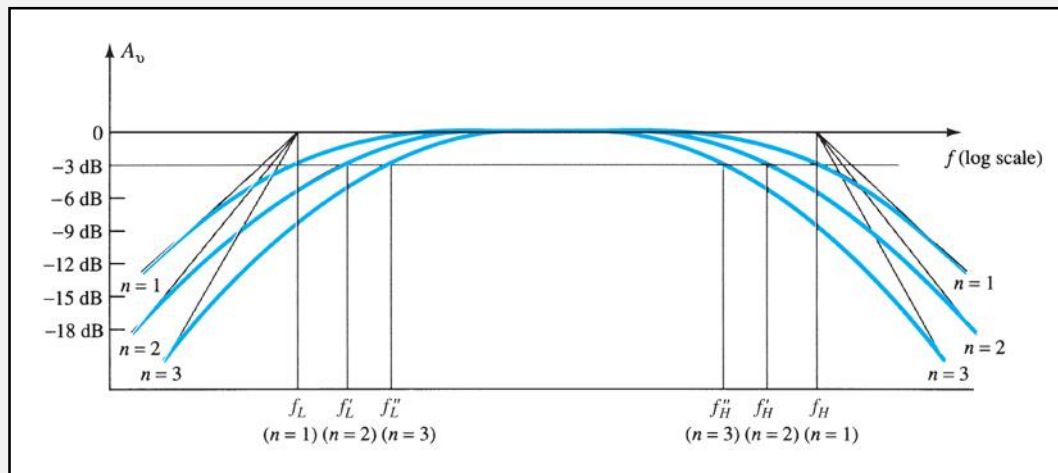


# Multistage Frequency Effects

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Each stage has its own frequency response, but the output of each stage is affected by capacitances in the subsequent stage. For example, the output capacitance ( $C_o$ ) is affected by the input Miller Capacitance ( $C_{Mi}$ ) of the next stage.

# Multistage Amplifier Response



Once the cutoff frequencies have been determined for each stage (taking into account the shared capacitances), they can be plotted.

Note the *highest* lower cutoff frequency ( $f_L$ ) and the *lowest* upper cutoff frequency ( $f_H$ ) are closest to the actual response of the amplifier.

# Square Wave Testing

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In order to determine the frequency response of an amplifier by experimentation, you must apply a wide range of frequencies to the amplifier.

One way to accomplish this is to apply a square wave. A square wave consists of multiple frequencies (by Fourier analysis: it consists of odd harmonics).

# Square Wave Response Waveforms

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If the output of the amplifier is not a perfect square wave then the amplifier is 'cutting' off certain frequency components of the square wave.